

Preparation of a Resistance Formula for Net-Tension Failure of Single and Multi-rowed Bolted Connections of Fibre-Polymer Composite

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Fibre-Polymer Composites in Construction (FPCC)

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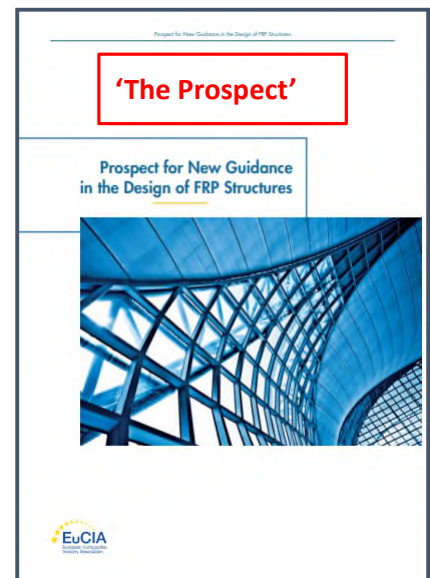
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Taster to Eurocode Project

STAGE 1: Ascione, L., Caron, J-F., Godonou, P., van IJselmuiden, K., Knippers, J., Mottram, T., Oppe, M., Gantriis Sorensen, M., Taby J. and Tromp, L., *Prospect for New Guidance in the Design of FRP*, JRC Science and Policy Report, Policy Framework Existing Regulations and Standards, JRC99714, EUR 27666 EN, European Union, Luxembourg. 2016 & 2017.

<https://tinyurl.com/yycmwzs4> (1 September 2022)
(free download)



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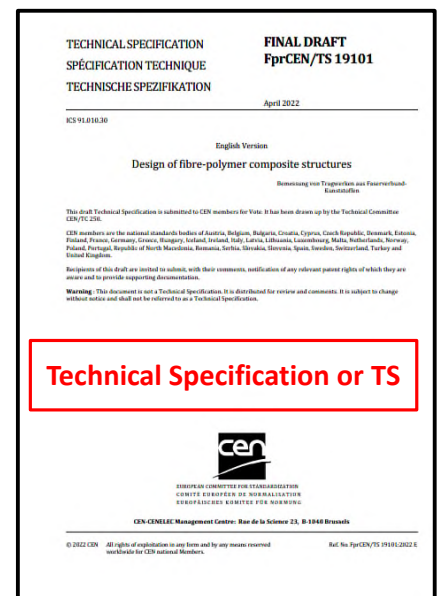
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Taster to Eurocode Project

STAGE 2: FprCEN/TS 19101 *Design of Fibre-Polymer Composite Structures*

Transforming STAGE 1 Prospect to be with:

- Basic of design (γ_M s, η_c s and $\phi(t)$ s);
- ULS of sandwich panels;
- Creep rupture;
- Fatigue;
- Detailing;
- Adhesive joints and connections;
- Structural fire design.



Technical Specification or TS



EUROPEAN COMMITTEE FOR STANDARDIZATION
COMITÉ EUROPÉEN DE NORMALISATION
EUROPAISCHES KOMITEE FÜR NORMUNG

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STAGE 2: FprCEN/TS 19101 *Design of Fibre-Polymer Composite Structures*

CEN Technical Specification (TS) has:

- adopted CEN's policy guidelines and procedures;
- taken into account and resolving comments from National Standard Bodies (NSBs) not incorporated in STAGE 1;
- revised paragraphs, clauses and subclauses that been identified to require improvements.

To accompany our TS there is:

- a **Background Document** of '1000' pages with a commentary to the important paragraphs, figures and tables;
- 16 **Worked Examples** covered over '300' pages
- A **National Annex** for National Determined Parameter and other national information.

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- | | |
|----------------------------------|---|
| 1. Scope | 10. Fatigue |
| 2. Normative reference | 11. Detailing |
| 3. Terms, definition and symbols | 12. Connections and joints |
| 4. Basic of design | Annex A (Informative) Creep coefficients |
| 5. Materials | Annex B (Informative) Indicative values of material properties for preliminary design |
| 6. Durability | Annex C (Informative) Buckling of orthotropic laminates and profiles |
| 7. Structural analysis | Annex D (normative) Structural fire design |
| 8. Ultimate limit states | Annex E (Informative) Bridge details |
| 9. Serviceability limit states | |



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Luigi Ascione, J. R. Correia, T. Keller, J. Knippers, J. T. Mottram, C. Paulotto and J. Sena-Cruz, '*Design of fibre-polymer composite structures - European Technical Specification: Overview and scope*,' in **Proceedings of 20th European Conference on Composite Materials (ECCM 20), 2022**, Paper 61551.

João R. Correia, J. Pacheco, J. D. Sorensen, T. Keller, J. T. Mottram, J. Sena-Cruz, '*Design of fibre-polymer composite structures – European Technical Specification: Basis of Design*,' *ibid*, Paper 61625.

José Sena-Cruz, M. Garrido Mário, J. R. Correia, J. Pedro, T. Keller, J. T. Mottram, '*Design of fibre-polymer composite structures – European Technical Specification: Temperature and moisture effects*,' *ibid*, Paper 61619.

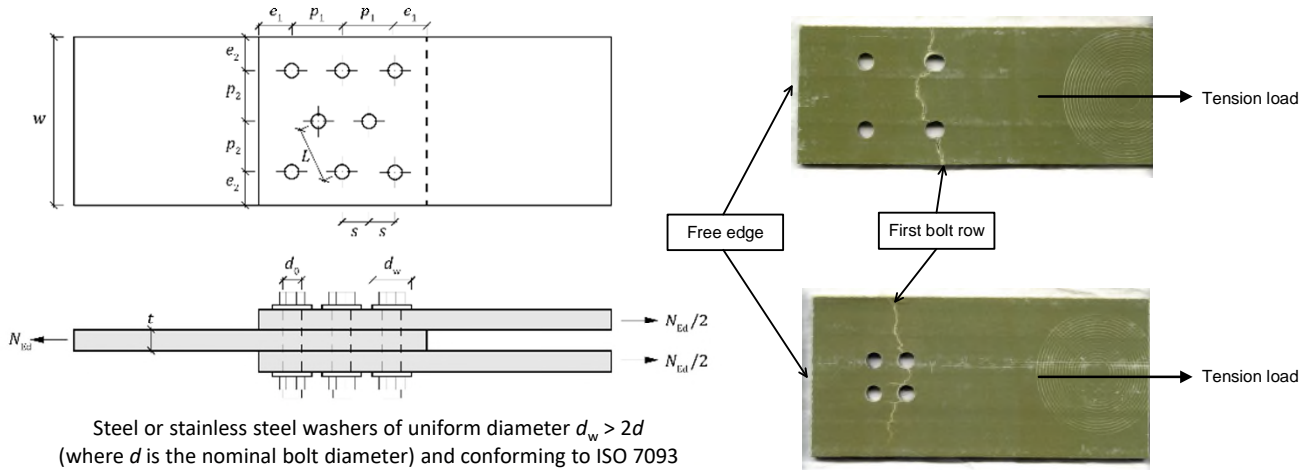
J. Toby Mottram, L. Tromp, M. Pavlovic, J. R. Correia, T. Keller and J. Sena-Cruz, '*Design of fibre-polymer composite structures – European Technical Specification: Combined stresses*,' *ibid*, Paper 61618.

Thomas Keller, J. R. Correia, J. T. Mottram, and J. Sena-Cruz, '*Design of fibre-polymer composite structures – European Technical Specification: Fatigue and detailing*,' *ibid*, Paper 61617.



Net-Tension Failure of Bolted Connections

Steel bolts (same diameter) no more than four rows and four columns of bolting, can be staggered



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Net-Tension Failure of Bolted Connections

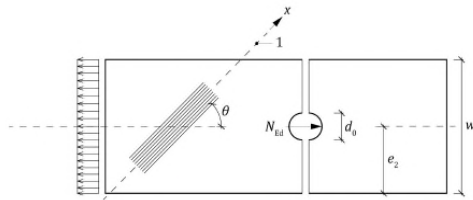
Table 11.1. Minimum requirements for bolted connection geometries (reproduced from TS)

Nominal bolt diameter (d) (recommended range)	$d \geq t_{\min}$ ($t_{\min} \leq d \leq 1.5 t_{\min}$)
Nominal bolt hole clearance	$d_0 - d \geq 1 \text{ mm}$
Distances between holes without staggered bolts	$p_1 \geq 4d; p_2 \geq 4d$
Distances between holes with staggered bolts	$p_1 \geq 4d; p_2 \geq 2d; L \geq 2.8d$
Distances from edges single row multi-rows	side $e_2 \geq 2d$ end $e_1 \geq 2.5d$ or $\geq 30\text{mm}$ end $e_1 \geq 2d$

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Net-Tension Failure of Bolted Connections

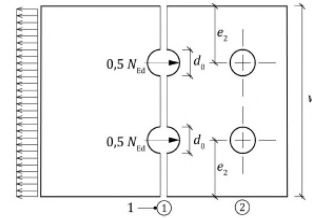
Formal vote version: **FprCEN/TS 19101:2022**



Key

1 principal direction of laminate or direction of pultrusion

Figure 12.2 — Net-tension failure mode illustrated with a single bolt, $n_{b,1} = 1$



Key

1 row No. (j)

Figure 12.3 — Net-tension failure mode illustrated with a 2×2 multi-bolted connection, $n_{b,1} = 2$

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Net-Tension Failure of Bolted Connections

12.2.3.1 Net-tension failure

IMPORTANT – Test results

(1) When the net-tension force is oriented at an angle $0^\circ \leq \theta \leq \pm 5^\circ$ to the x direction of pultruded profiles or pultruded flat laminates of constant thickness (see Figures 12.2 and 12.3), its design value, N_{Ed} , for net-tension failure should satisfy the condition in Formula (12.3):

where

$N_{x,nt,Rd}$ is the design value of the net-tension resistance in the x direction, given by Formula (12.4),

$$N_{x,nt,Rd} = \frac{1}{k_{tc}} \cdot (w - n_{b,1} \cdot d_0) \cdot t \cdot f_{x,t,d} \quad (12.4)$$

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Net area tension strength of composite

In 'The Prospect' $k_{tc} = 3,75$

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Net-Tension Failure of Bolted Connections

where

- w is the width of the component ($w \geq 4d$, from Table 11.1), see also 12.2.3.1(5);
- $n_{b,1}$ is the number of bolts across the first bolt row (Row 1) where the net-tension failure mode occurs (see Figures 12.2 and 12.3);
- d_0 is the nominal bolt hole diameter;
- t is the laminate thickness;
- k_{tc} is a stress concentration factor that should be taken from Table 12.2 for specific bolted connection configurations that satisfy the geometry requirements in Table 11.1; for other bolted connection configurations, k_{tc} should be taken equal to 3,0;
- $f_{x,t,d}$ is the design value of the tensile strength of the pultruded laminate in the x direction, given by Formula (12.5),

In 'The Prospectus' $k_{tc} = 3,75$

$$f_{x,t,d} = \frac{\eta_c}{\gamma_m \cdot \gamma_{Rd}} \cdot f_{x,t,k} \quad (12.5)$$

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Net-Tension Failure of Bolted Connections

$$f_{x,t,d} = \frac{\eta_c}{\gamma_m \cdot \gamma_{Rd}} \cdot f_{x,t,k} \quad (12.5)$$

e.g., Moisture $\eta_{cm} = 0,85$ (Exposure Class II) and temperature $\eta_{ct} = 0,9$

e.g., $\gamma_m = 1,15$ ($V_x = 0.1$) and $\gamma_{Rd} = 1,50$ (calibrated using test results with ISO 2394 Annex C, Section C.6 & prEN 1990, Annex D)

where

- γ_m is defined in 4.4.5 (to be selected for $f_{x,t,k}$);
- γ_{Rd} is defined in 4.4.6 (Table 4.5, Net-tension failure);
- η_c is defined in 4.4.7 (to be selected for $f_{x,t,k}$);
- $f_{x,t,k}$ is the characteristic value of the tensile strength of the pultruded laminate material in the x direction.

EN ISO 527 (all parts), Plastics – Determination of tensile properties

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Net-Tension Failure of Bolted Connections

Table 12.2 — Values of stress concentration factor k_{tc} for specified bolted connection configurations when N_{Ed} is oriented with an angle $0^\circ \leq \theta \leq \pm 5^\circ$ to the major principal axis (x direction) of pultruded laminates with glass fibres

Bolted connection configuration	k_{tc}
Single	2,0
1 × 2 (single row)	2,5
2 × 1 (single column)	2,5
1 × 3	2,5
3 × 1	2,5
2 × 2	2,0
3 × 3	1,5
1 × 1 (staggered)	2,0
2 × 2 (staggered)	2,0

<< 3,75

<< 3,75

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Net-Tension Failure of Bolted Connections

Bolt configuration	Rosner [6] or Hassan [7]	Lutz [5] ¹ or Wang [8] or Turvey [9]	Prabhakaran Razaqa & Devara [10]	Matharu [11]	k_{tc} in Formula (12.4)
(1)	(2)	(3)	(4)	(5)	(6)
Single	1,0-1,6	1,5-1,6; 1,5			2,0
1x2 (single row)	0,9-2,0	1,3-2,3; 1,6-2,2		1,5-1,8	2,5
2x1 (single column)	1,0-1,9	1,3-2,2	1,7	1,7	2,5
1x3	1,1-2,0				2,5
3x1	1,4-2,4				2,5
2x2	1,0-1,6	1,3-1,9; 1,4-2,1	1,8	1,2-1,3	2,0
3x3		1,2-1,4			1,5
1x1 (staggered)				1,9	2,0
2x2 (staggered)			2,1; 1,8; 2,1		2,0

Based on Mean and NOT characteristic values

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Concluding Remarks

1. What a milestone has been achieved with the publication (SOON) of the Eurocode CEN Technical Specification (**CEN/TS 19101** – passed the Formal Vote step) and its accompanying Background Document and Worked Examples.
2. All National Standard Bodies (NSBs) requirements were met when transforming '*The Prospect*' into the TS.
3. A pragmatic design procedure based on a semi-empirical formula has been prepared that determines the resistance of bolted-connections of fibre-polymer composites.
4. For efficient designs the constant 'stress concentration' factor of 3,75 in '*The Prospect*' has been replaced with values of 1,5, 2,0 or 2,5 and 3,0 for different connection configurations; thereby making detailing more efficient and cheaper.

Acknowledgements



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- WG4.T2** and WG4 colleagues: [João R. Correia](#) (Leader); [Thomas Keller](#); [Jan Knippers](#); [José Sena-Cruz](#); [Carlo Paulotto](#); Matthias Oppe; Luigi Ascione.

Hit me with your Questions?

