

# WORK PACKAGE 1.2

# FUEL CELLS

## LOUGHBOROUGH UNIVERSITY

Team:

Rob Thring  
Nick McCarthy  
Jiayi Gu

Date:

14 Jan 2015

**EPSRC**

Pioneering research  
and skills



*Cranfield*  
UNIVERSITY

Loughborough  
University

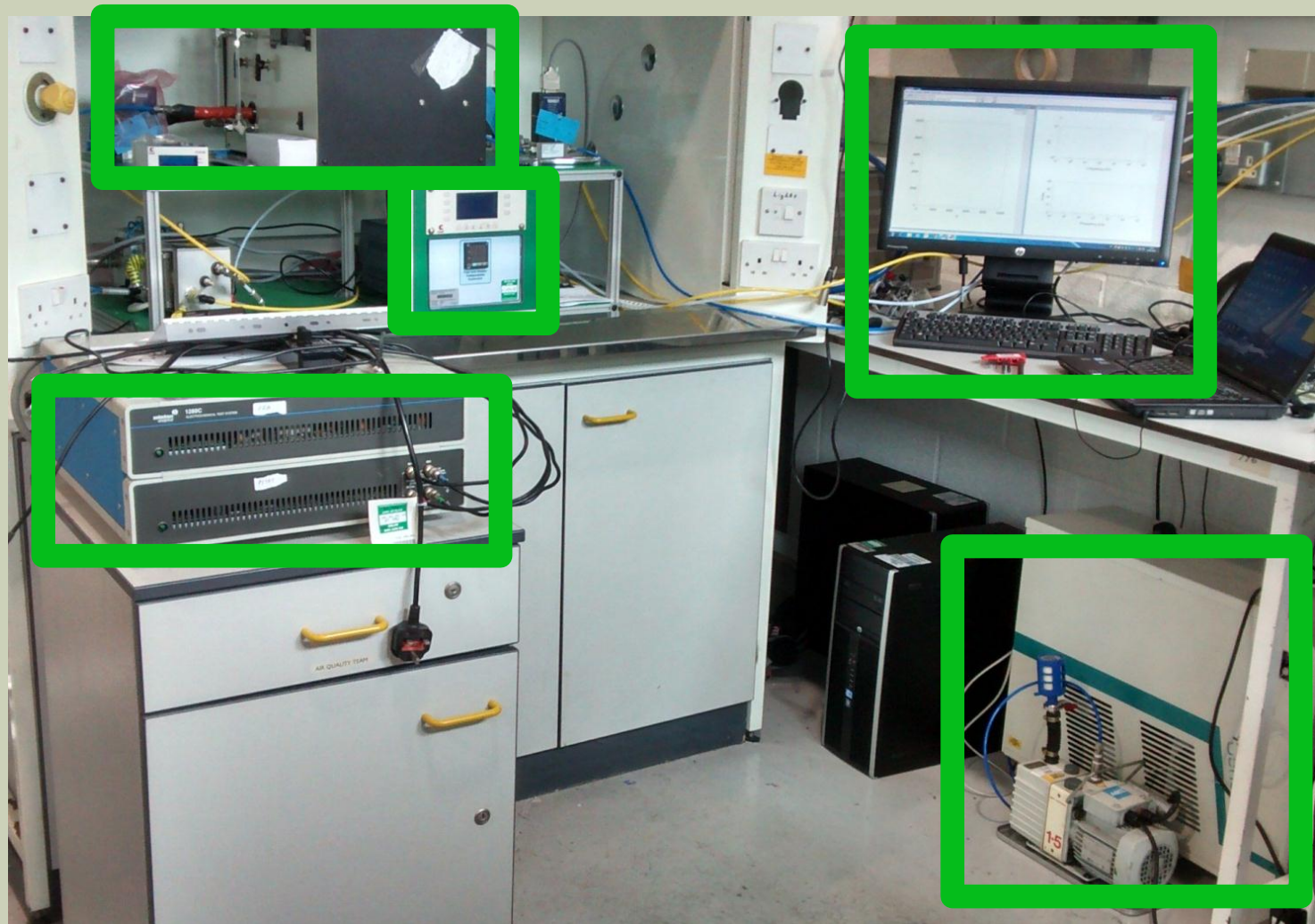
Imperial College  
London



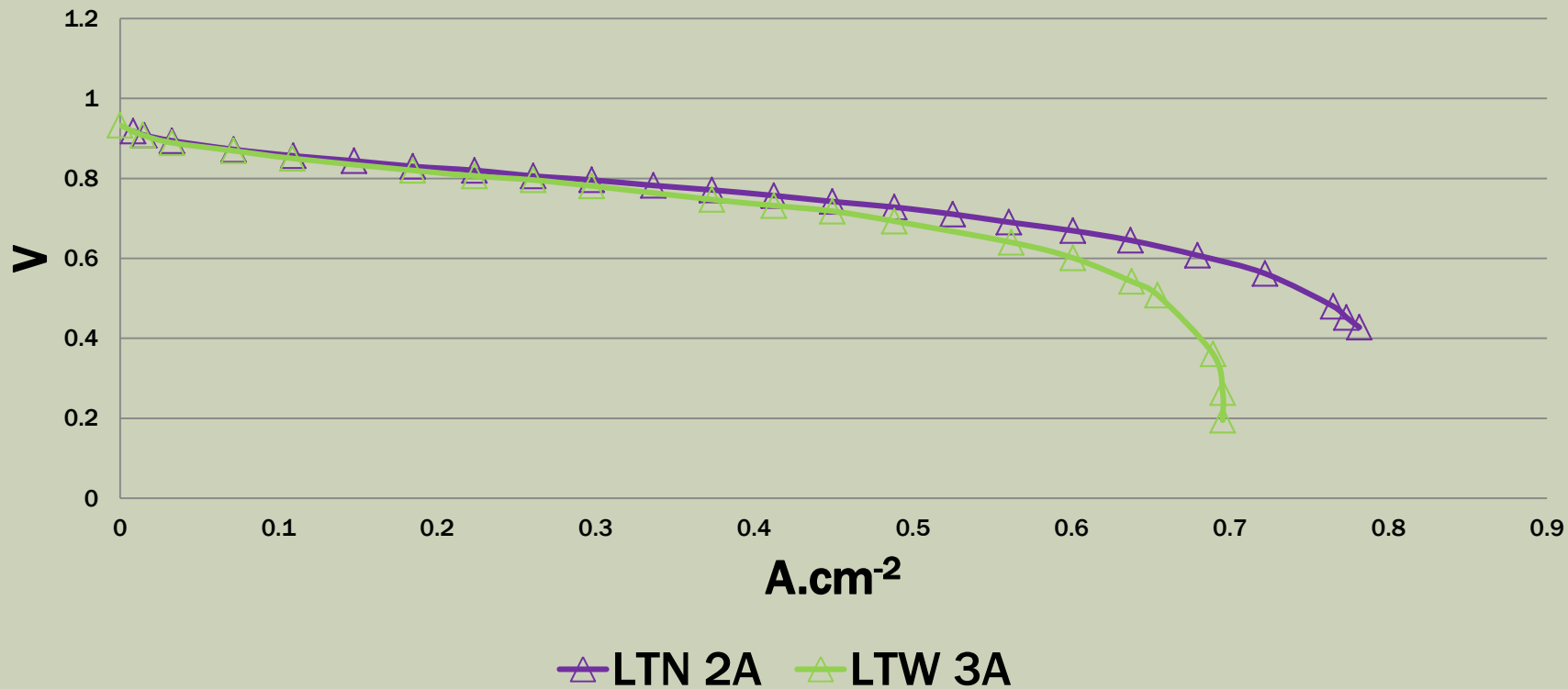
# Experimental work

By Nick McCarthy

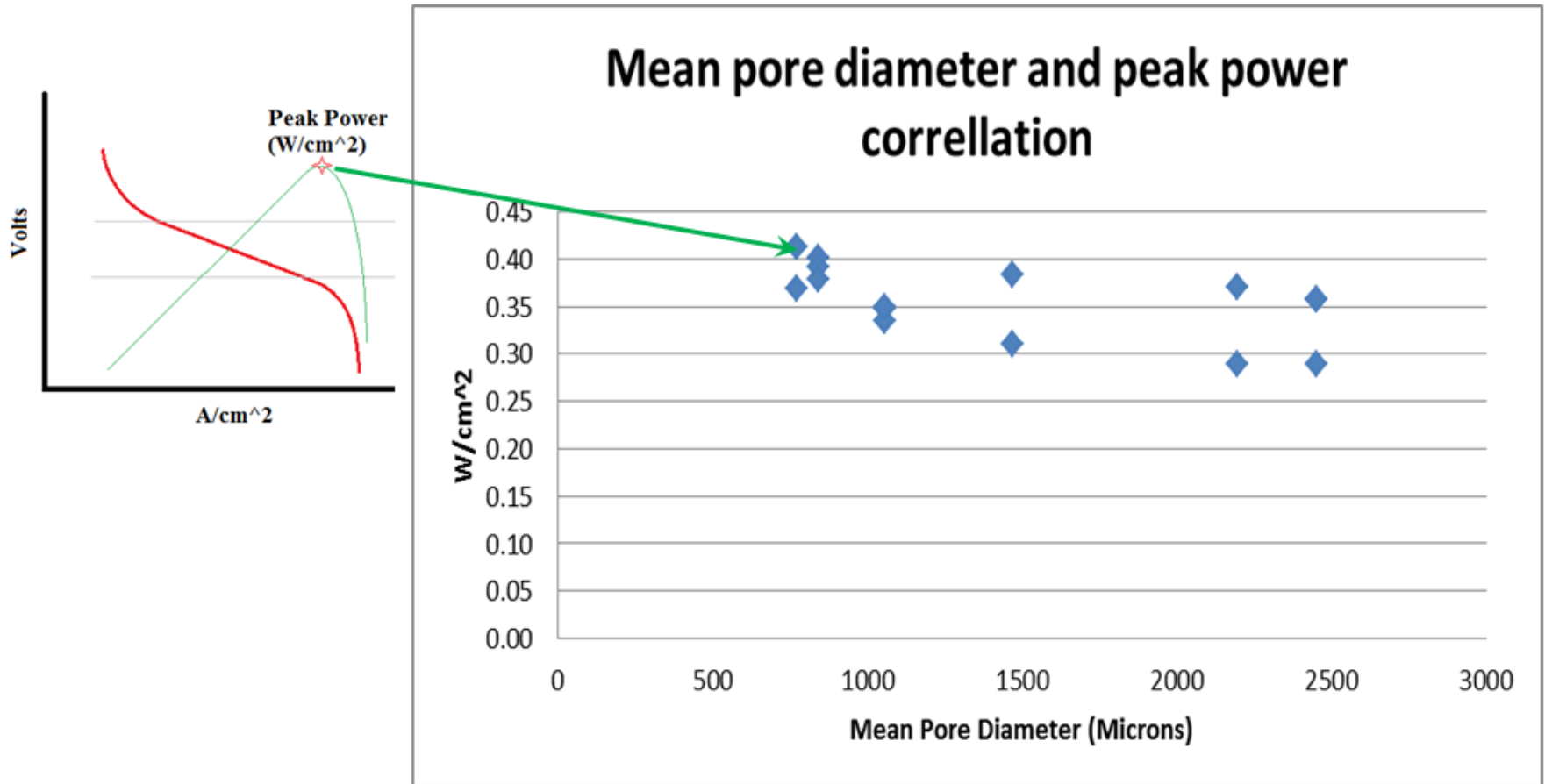
# G.E.I.S.T. RIG AT L'BORO



## Uniform 0.4mg/cm<sup>2</sup> Pt on Cathode Non-Woven (LTN) and Woven (LTW) Comparison Polarisation curves



# MULTIPLE GDL TYPES (PAPER, WOVEN, NON-WOVEN) POROSITY AND PEAK POWER PERFORMANCE



# EMPIRICAL LINEAR MODEL (WMAX AND GDL RELATIONSHIP)

| Coefficients:          |            |            |         |          |     |
|------------------------|------------|------------|---------|----------|-----|
|                        | Estimate   | Std. Error | t value | Pr(> t ) |     |
| (Intercept)            | 0.4922468  | 0.0527059  | 9.339   | 5.55E-14 | *** |
| H <sub>2</sub> O angle | -0.0003779 | 0.0002174  | -1.739  | 0.08644  | .   |
| MPL Mod'               | 0.0398119  | 0.0103118  | 3.861   | 0.000247 | *** |
| PTFE wt%               | -0.2254306 | 0.0731867  | -3.08   | 0.002942 | **  |
| RH%                    | -0.0011252 | 0.0004949  | -2.274  | 0.026019 | *   |
| Structure Mod          | -0.0141882 | 0.0083572  | -1.698  | 0.093942 | .   |
| % pores                | -0.0014299 | 0.0003463  | -4.129  | 9.81E-05 | *** |

Which we can simplify to

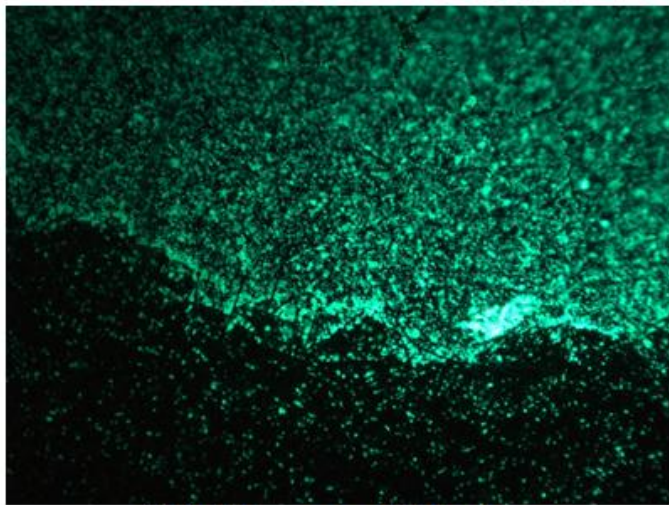
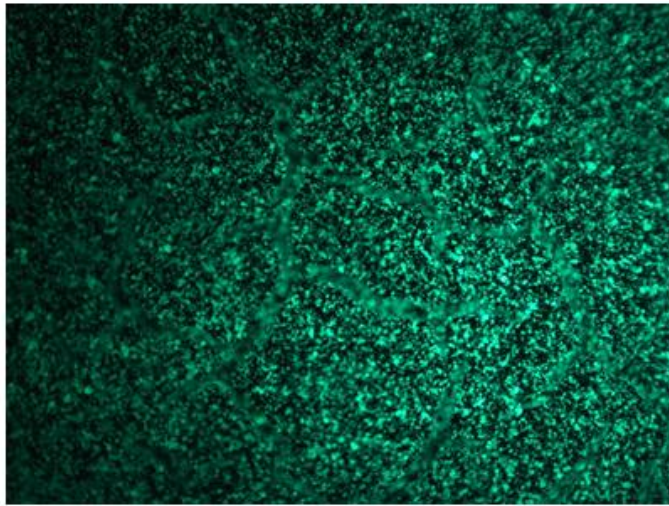
$$W_{MAX} = 0.492 + 0.040k_{MPL} - 0.225PTFE_{(wt\%)} - 0.001\% \text{ porosity}$$

Where

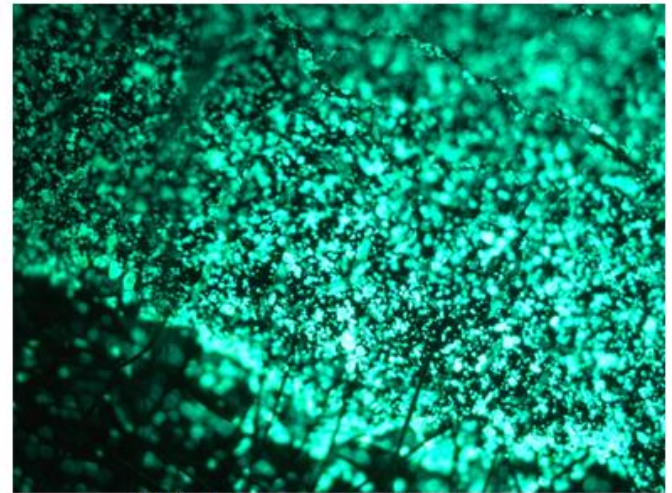
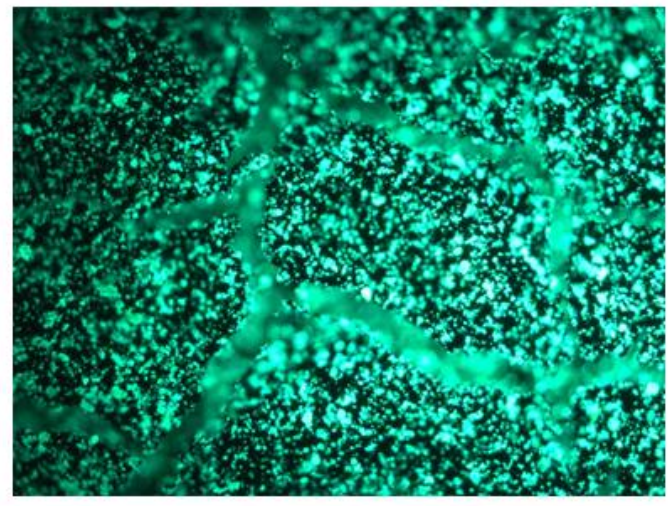
$k_{MPL} = 0$  for no MPL and 1 for fuel cells that include an MPL



# FLUORESCENT DOPING OF PT AND INK DISTRIBUTION



1% FI-cene 50\*mag

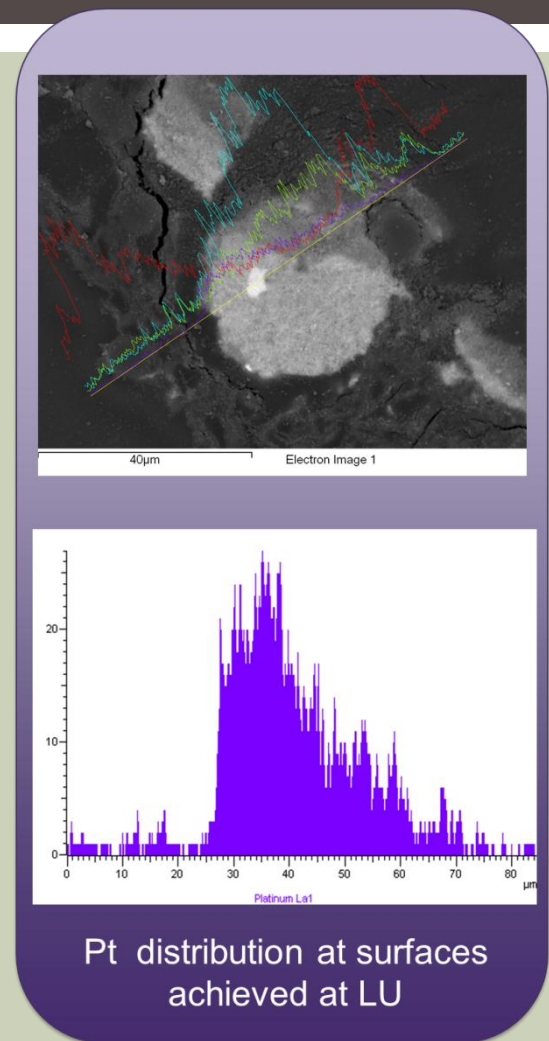
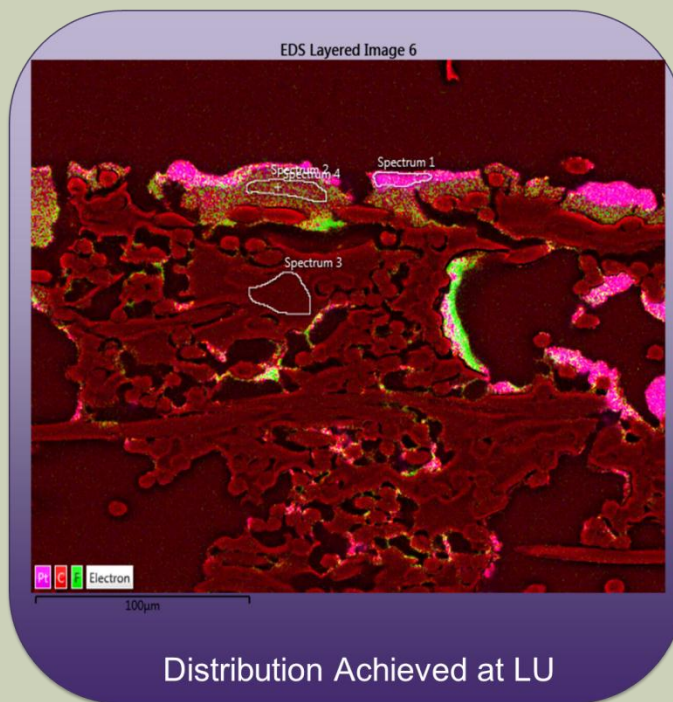


1% FI-cene 100\*mag

# MODELLED VS ACTUAL PT DISTRIBUTION IN LAYERED CATALYSTS

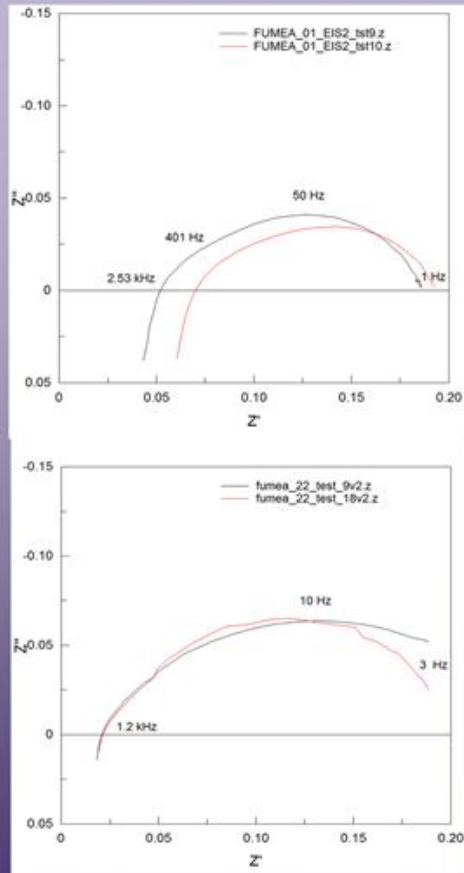


Proposed distribution in [4]

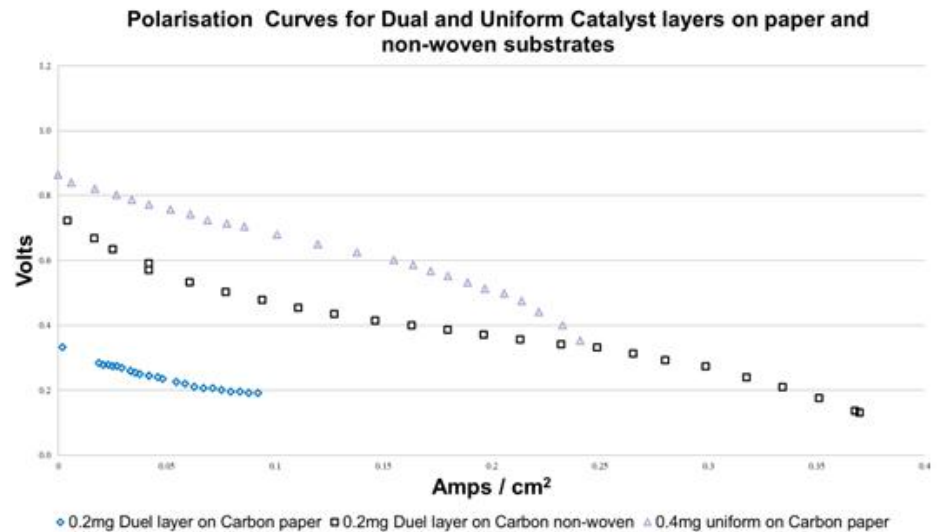




# INITIAL DUEL LAYER RESULTS AND MASS LIMITING ISSUES



Dehydration of duel layer (FUMEA\_01) system during EIS



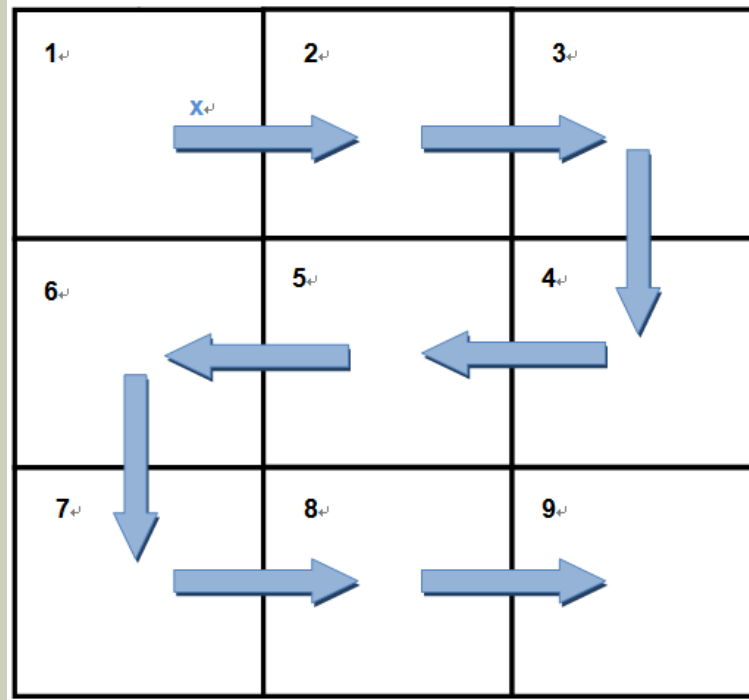
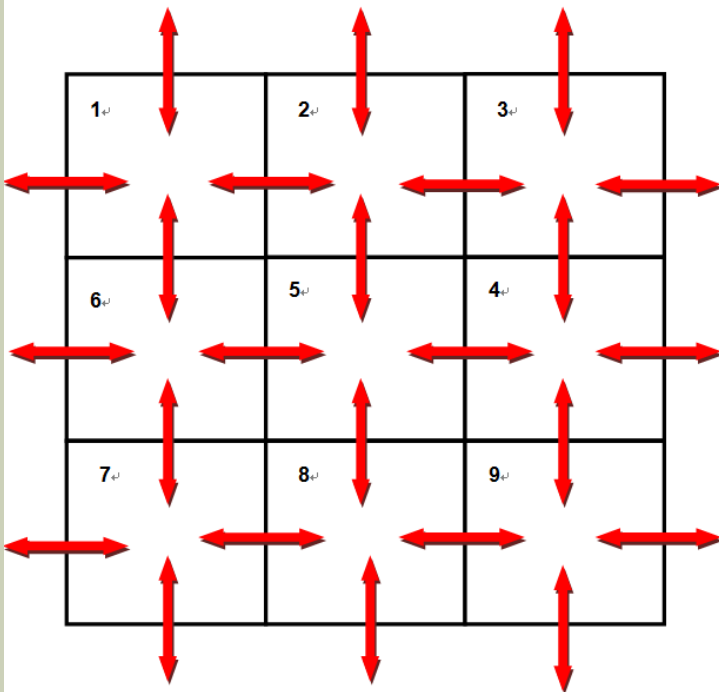
# REFERENCES

[1] Xie et al.;2005; Functionally Graded Cathode Catalyst Layers for Polymer Electrolyte Fuel Cells: II. Experimental Study of the Effect of Nafion Distribution; Journal of the Electrochemical Society, 152(6), pp. A1171-A1179

# Modelling work

By Jiayi Gu

# MODELLING PHILOSOPHY



Anode:  $\frac{d[\text{H}_2][\text{CO}][\text{H}_2\text{O}][\text{N}_2]}{dX_a}$

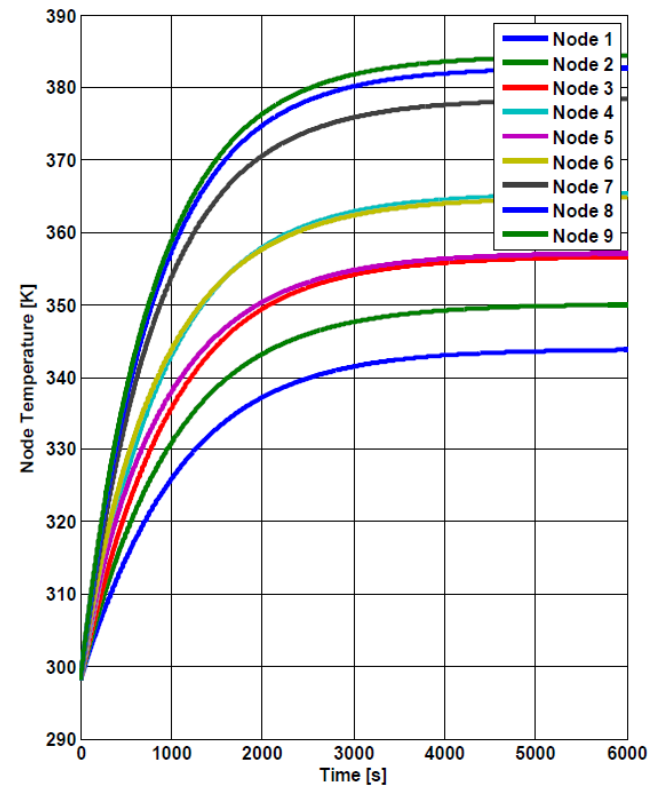
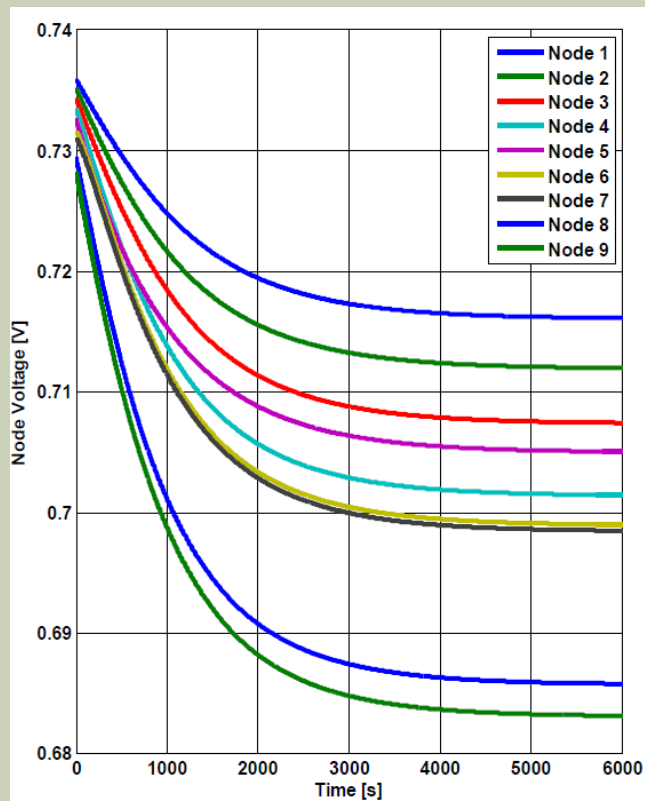
Cathode:  $\frac{d[\text{O}_2][\text{H}_2\text{O}][\text{N}_2]}{dX_c}$

Membrane:  $\frac{d[\text{H}_2\text{O}]}{d\delta_m}$

- To reveal the distributed characteristics of PEM fuel cells.
- 1-D fuel cell model discretised along the gas channel.
- Single serpentine gas channel.
- Thermal connections: internal + external.

# NODAL THERMAL PROPERTIES

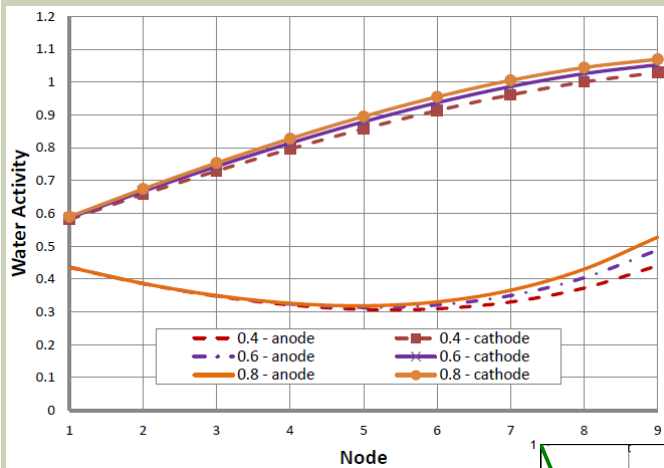
- Open cathode + dead-ended anode
- Cooling is provided by cathode air flow.



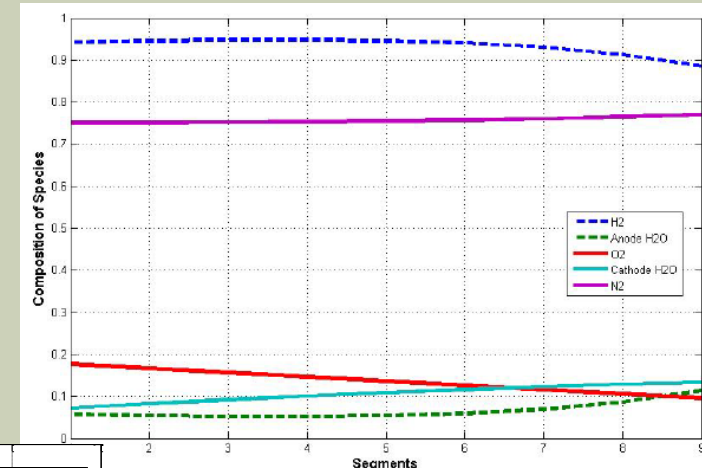


# WATER MANAGEMENT

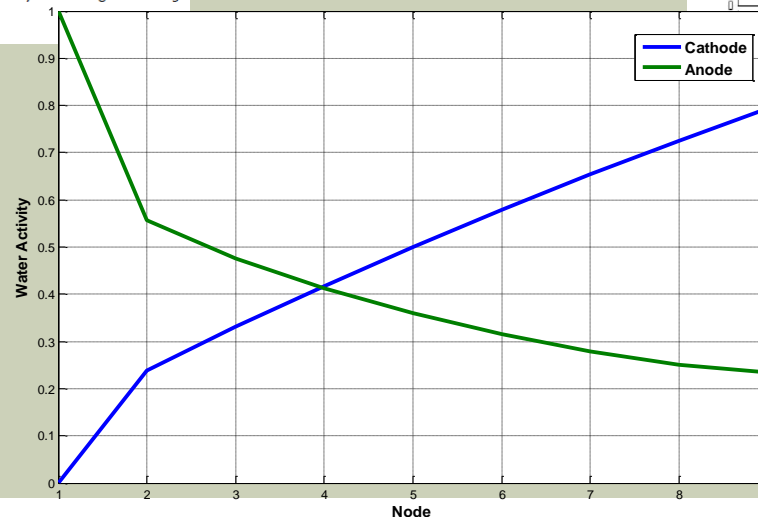
- Through-membrane water transport: Electro-osmotic drag and Back-diffusion.



[Above] Nodal humidity variations at different loads.

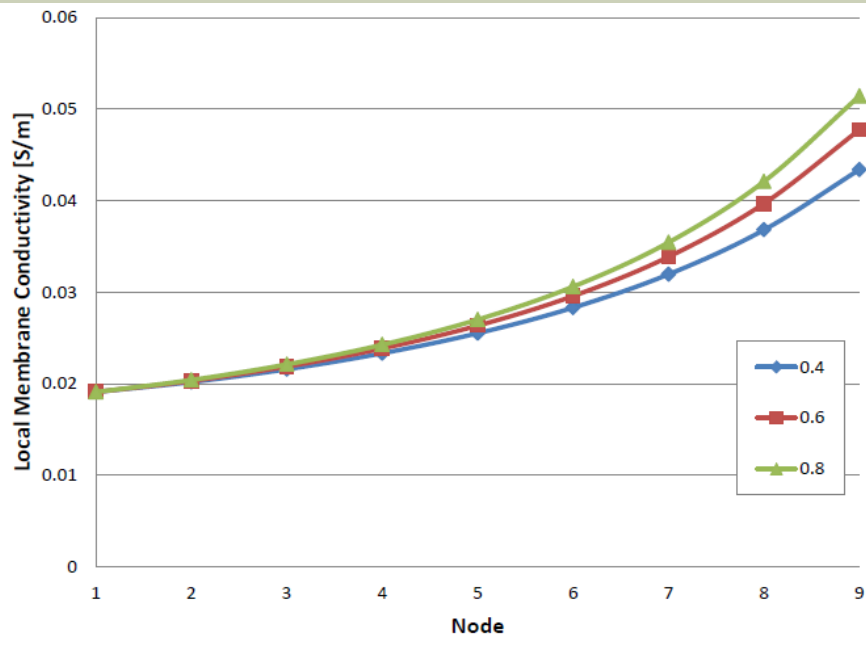


[Above] Species variations at 0.8A/cm<sup>2</sup>.



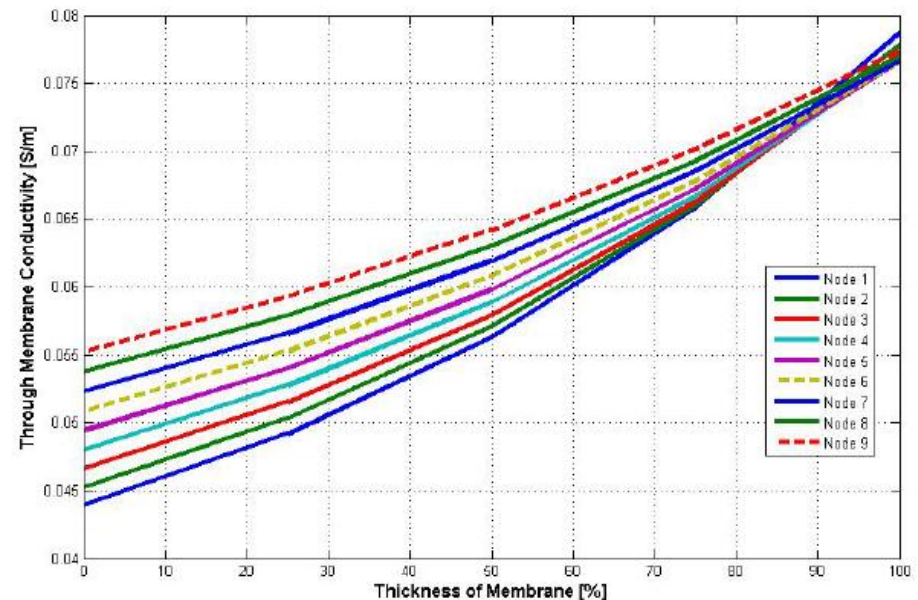
[Left] Extreme case: Fully humidified anode and dry cathode input.

# LOCAL MEMBRANE CONDUCTIVITY



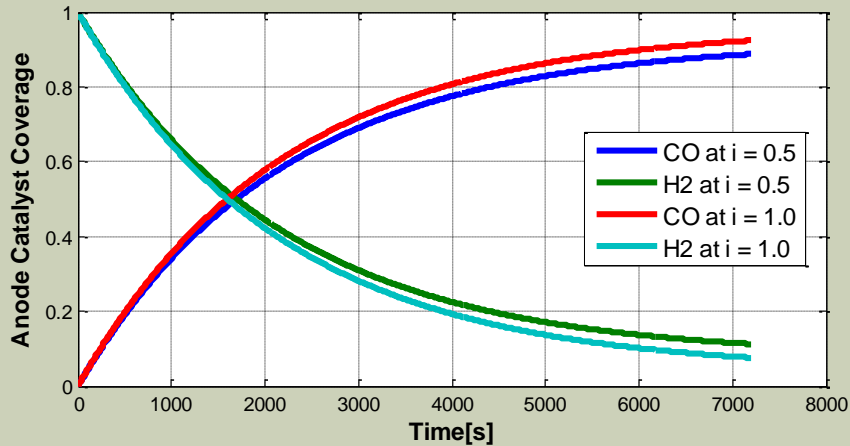
[Left] Local conductivity is a function of membrane water content.

[Right] Through-membrane conductivity is lower at anode surface and higher at cathode surface.

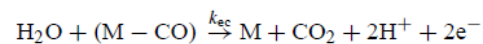
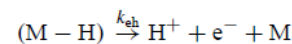
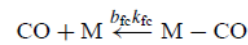
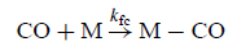
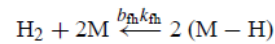
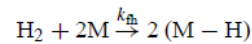
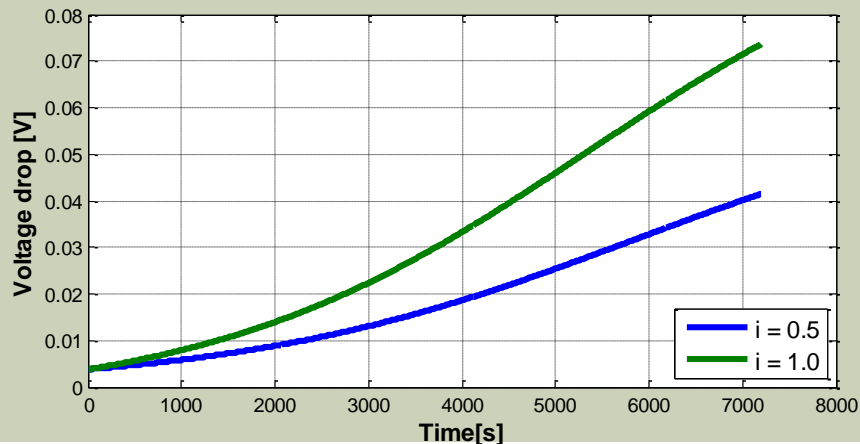


# DEGRADATION 1

## Carbon-monoxide Poisoning



- The adsorption, desorption and electro-oxidation of hydrogen and CO on the catalyst surface are described by a 6-reaction set<sup>2</sup>.
- The rate of change of coverage by hydrogen and CO is calculated by a set of kinetic equations in the of the Butler-Volmer equation.

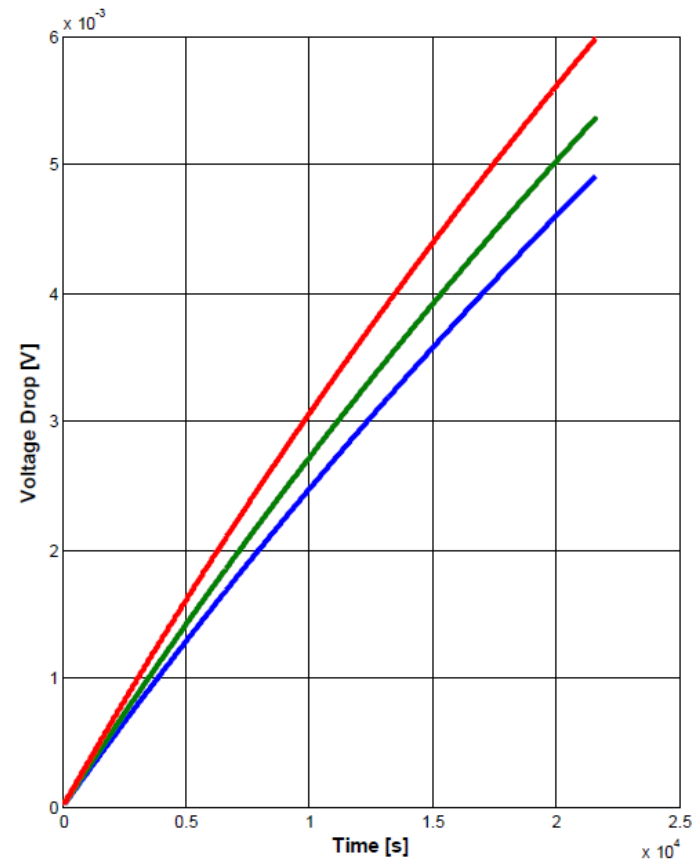
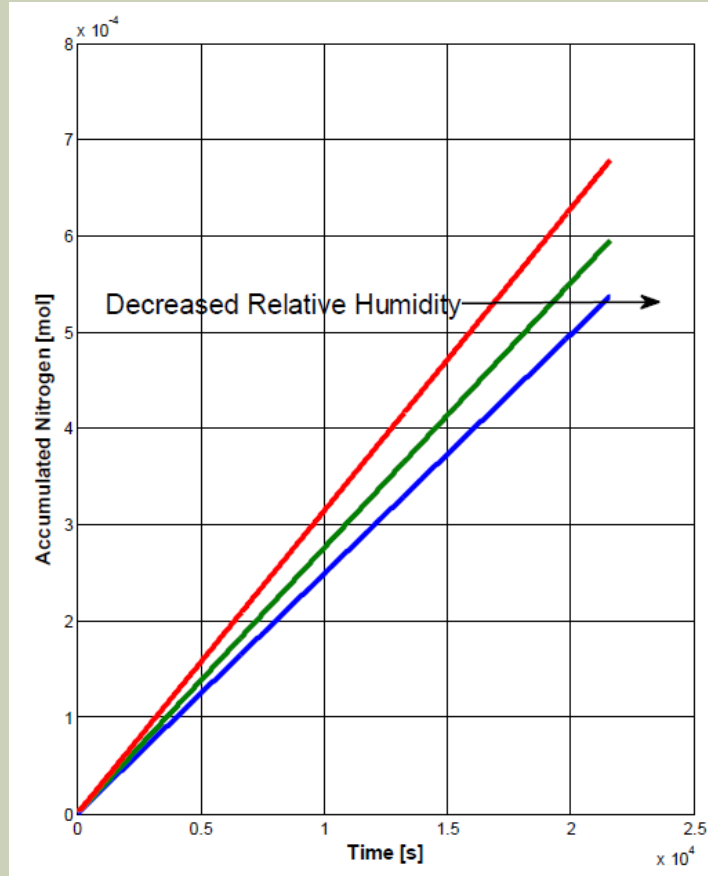


$$\rho \frac{d\theta_{\text{h}}}{dt} = k_{\text{fh}}x_{\text{h}}P(1 - \theta_{\text{h}} - \theta_{\text{c}}) - b_{\text{fh}}k_{\text{fh}}\theta_{\text{h}} - 2k_{\text{eh}}\theta_{\text{h}} \sinh\left(\frac{\eta_{\text{a}}}{RT/\alpha F}\right)$$

$$\rho \frac{d\theta_{\text{c}}}{dt} = k_{\text{fc}}x_{\text{c}}P(1 - \theta_{\text{h}} - \theta_{\text{c}}) - b_{\text{fc}}k_{\text{fc}}\theta_{\text{c}} - 2k_{\text{ec}}\theta_{\text{c}} \sinh\left(\frac{\eta_{\text{a}}}{RT/\alpha F}\right)$$

# DEGRADATION 2

- $N_2$  permeability in water is up to two magnitude higher than in Nafion.



# THANK YOU FOR YOUR TIME!

**Contact:**

[J.Gu2@lboro.ac.uk](mailto:J.Gu2@lboro.ac.uk)

[N.Mccarthy@lboro.ac.uk](mailto:N.Mccarthy@lboro.ac.uk)

[www.futurevehicles.ac.uk](http://www.futurevehicles.ac.uk)

