

# **FUTURE Vehicles WP3.1 – Developments in Reduced Order Modelling**

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**Dr Małgorzata Sumińska**  
Control Theory and Applications Centre  
Coventry University

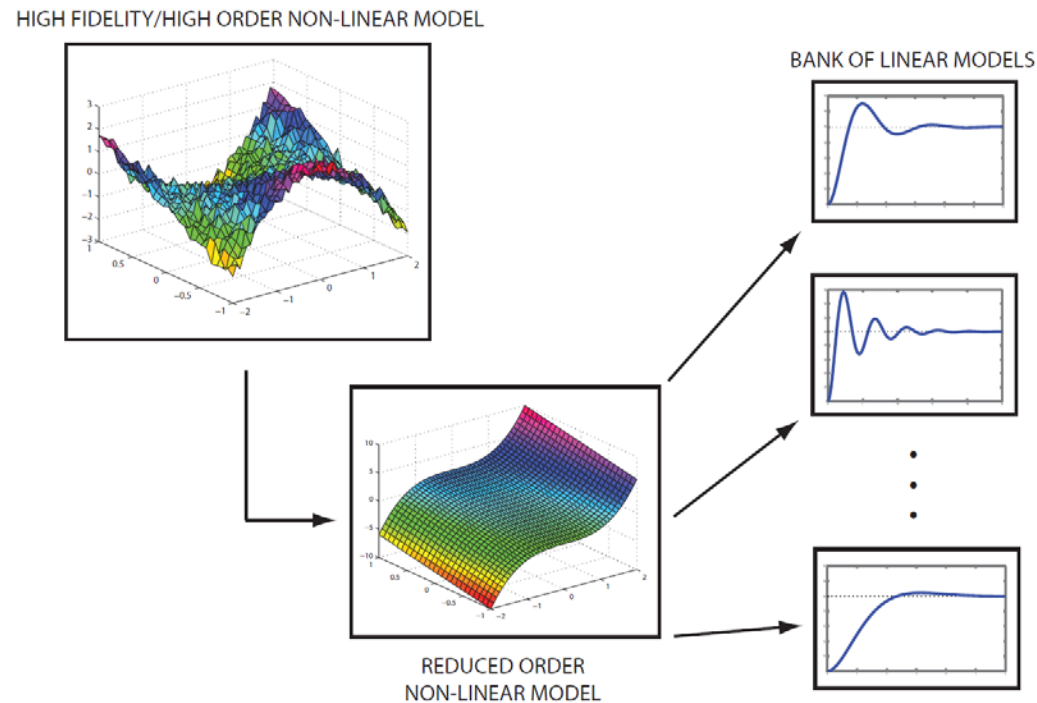
# Content



- Introduction
- Overview of reduced order modelling
  - > Features
  - > Requirements
- Case studies of reduction via **mathematical manipulation**
  - > Supercapacitor model
  - > Transmission line model
- Case studies of reduction via the **data driven approach**
  - > Electric machine
  - > Battery
- Summary

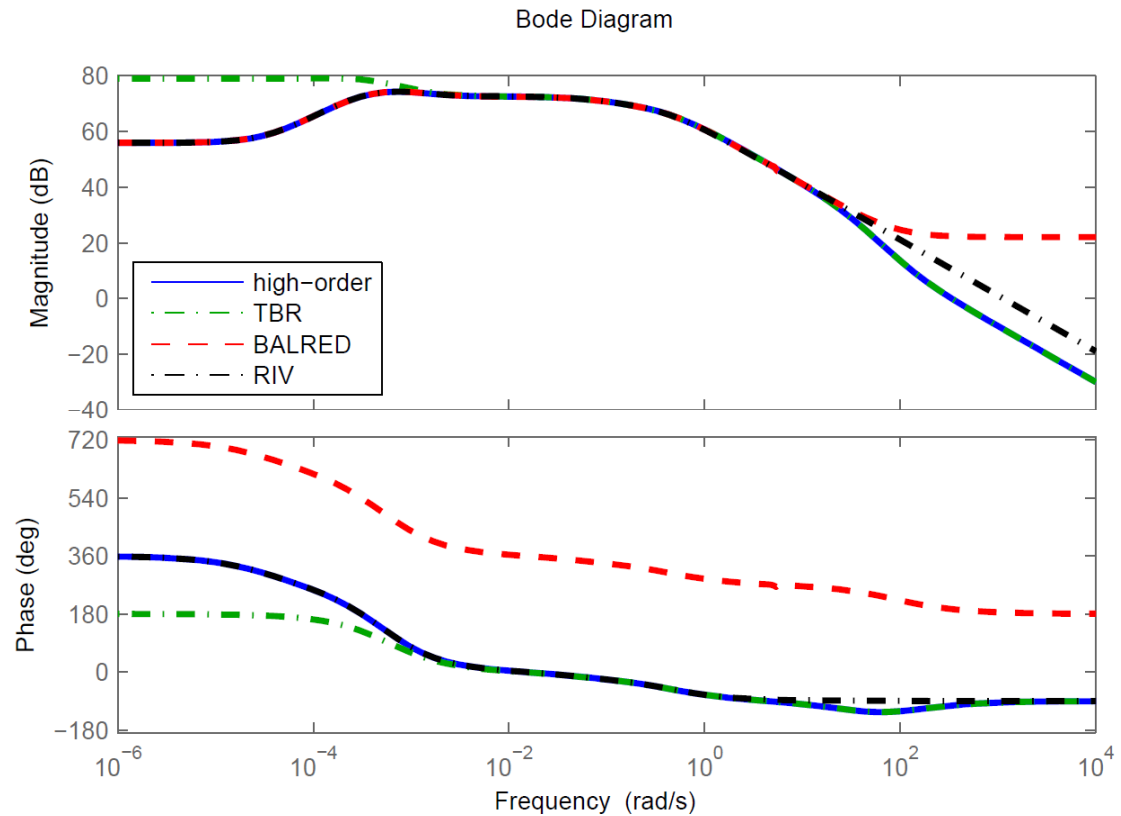
# Introduction

- Aim – to reduce computational complexity of model yet retain sufficient accuracy for a specific purpose, i.e. control, diagnostics, prognostics



# Overview of reduced order modelling

- Model features
  - > Dynamics
  - > Non-linearity
- Requirements
  - > Purpose of model
  - > Accessibility
  - > Accuracy
  - > Operational range
  - > Frequency range
- Features and requirements inform and define the model reduction problem



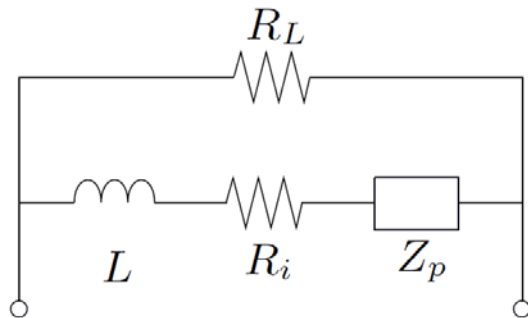
# Overview of techniques



- Classical approach
  - > Linear methods
    - Truncated balanced residualisation (TBR)
    - Singular perturbation analysis (SPA)
    - Krylov subspace methods
  - > Non-linear methods
    - Quadratic approximation
    - Trajectory piecewise linear approximation
- Data driven approach
  - > Parameter estimation and system identification methods
    - Estimation rules – least squares, recursive least squares, refined instrumental variables (RIV), Kalman filter for parameter estimation
    - Model structures – autoregressive, Box Jenkins, bilinear, Wiener, Hammerstein, state dependent parameter

# Case study: Supercapacitor

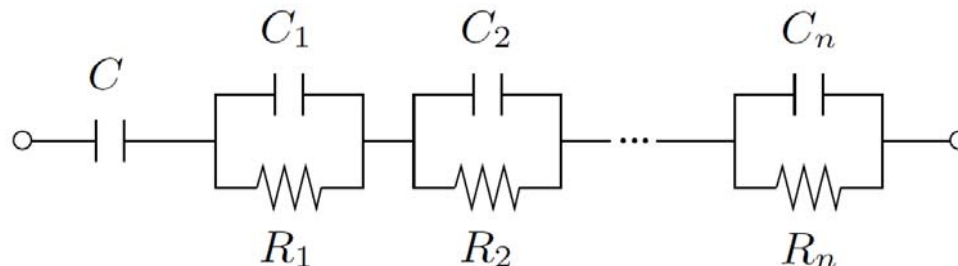
- Equivalent circuit of supercapacitor



$$Z_p(j\omega) = \frac{\tau \coth(\sqrt{j\omega\tau})}{C\sqrt{j\omega\tau}}$$

- $Z_p$  - complex pore impedance
- $C$  - capacitance
- $\tau$  - time constant
- $L$  - inductance
- $R_L$  - leakage resistance

- Complex pore impedance approximated by  $n$  RC branches in series with capacitor



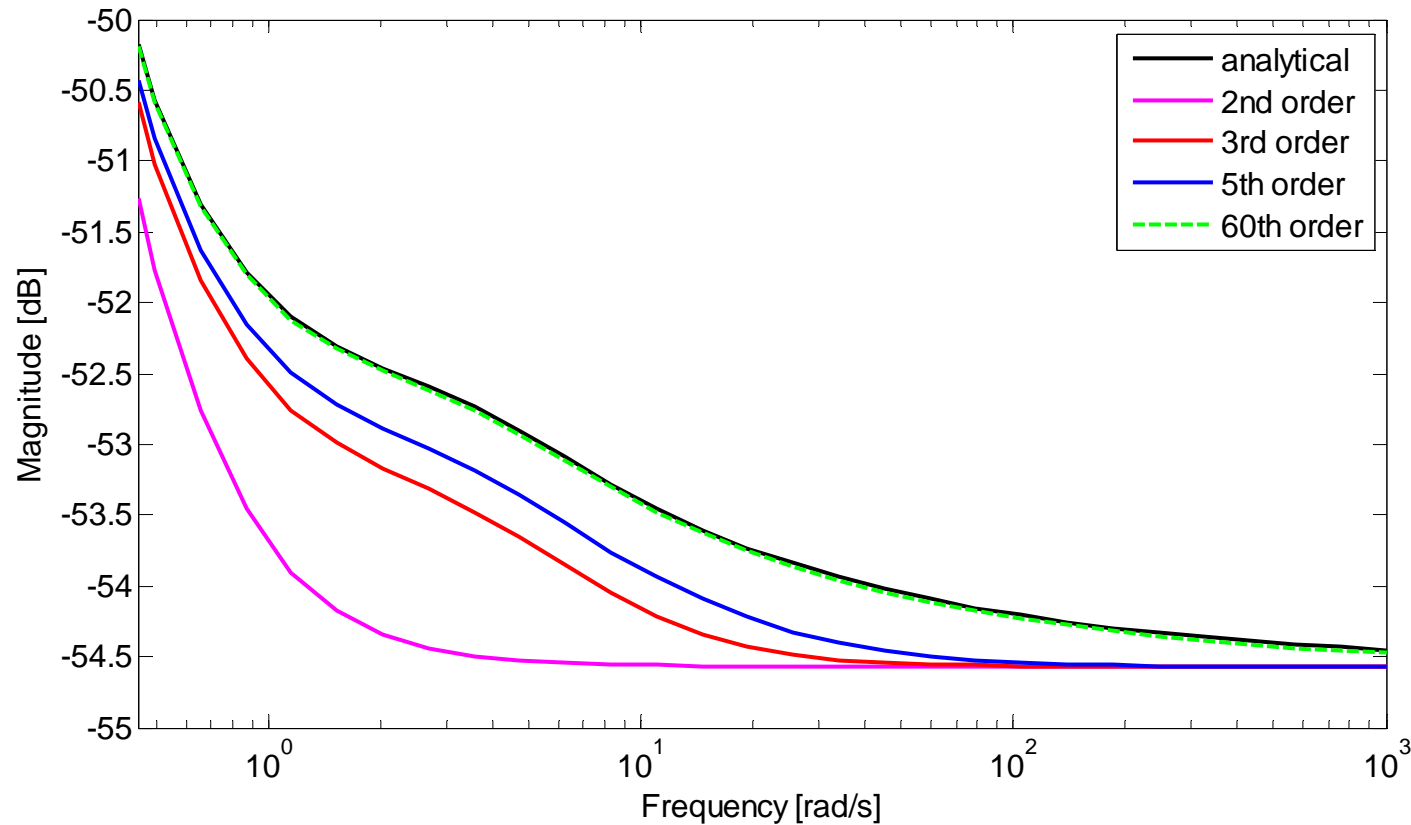
$$C_k = \frac{C}{2}$$

$$R_k = \frac{2\pi}{\pi^2 k^2 C} \quad k = 1, 2, \dots, n$$

model order =  $n+2$

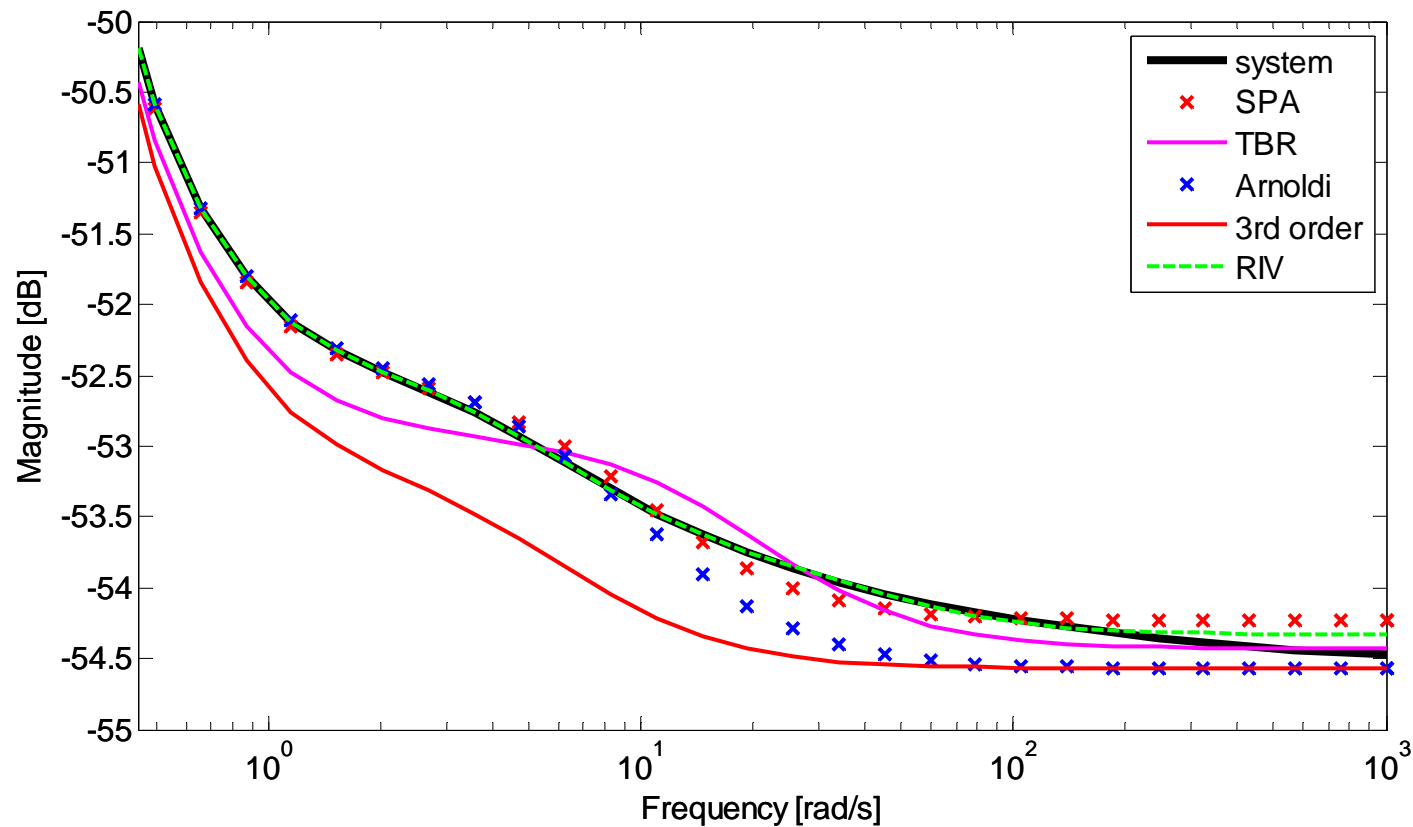
# Case study: Supercapacitor

- Accuracy of  $n$ -branch model
- 58-branch (60 order) model used as baseline for model order reduction (MOR)



# Case study: Supercapacitor

- Comparison of 3<sup>rd</sup> order model variants obtained via selected reduced order modelling techniques

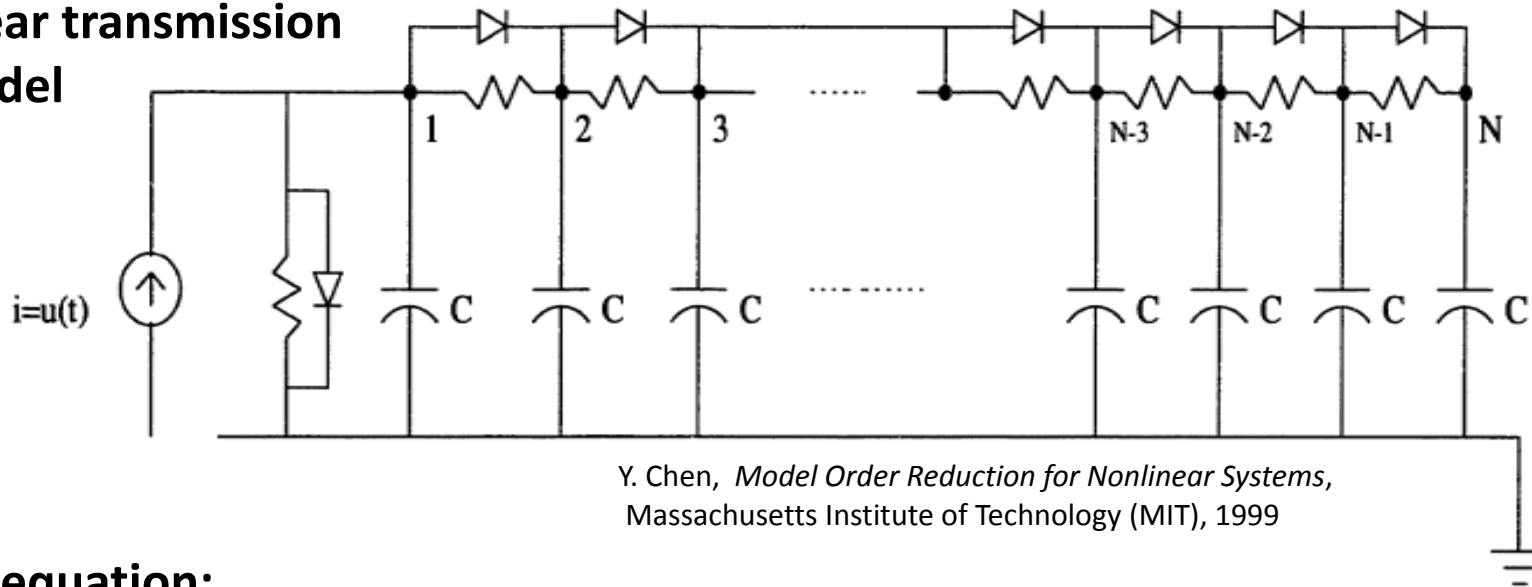




# Case study: Transmission line model



## Nonlinear transmission line model



Y. Chen, *Model Order Reduction for Nonlinear Systems*, Massachusetts Institute of Technology (MIT), 1999

## System equation:

$$C \frac{dv}{dt} = \begin{bmatrix} -g(v_1) - g(v_1 - v_2) \\ g(v_1 - v_2) - g(v_2 - v_3) \\ \vdots \\ g(v_{k-1} - v_k) - g(v_k - v_{k+1}) \\ \vdots \\ g(v_{N-1} - v_N) \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix} u(t)$$

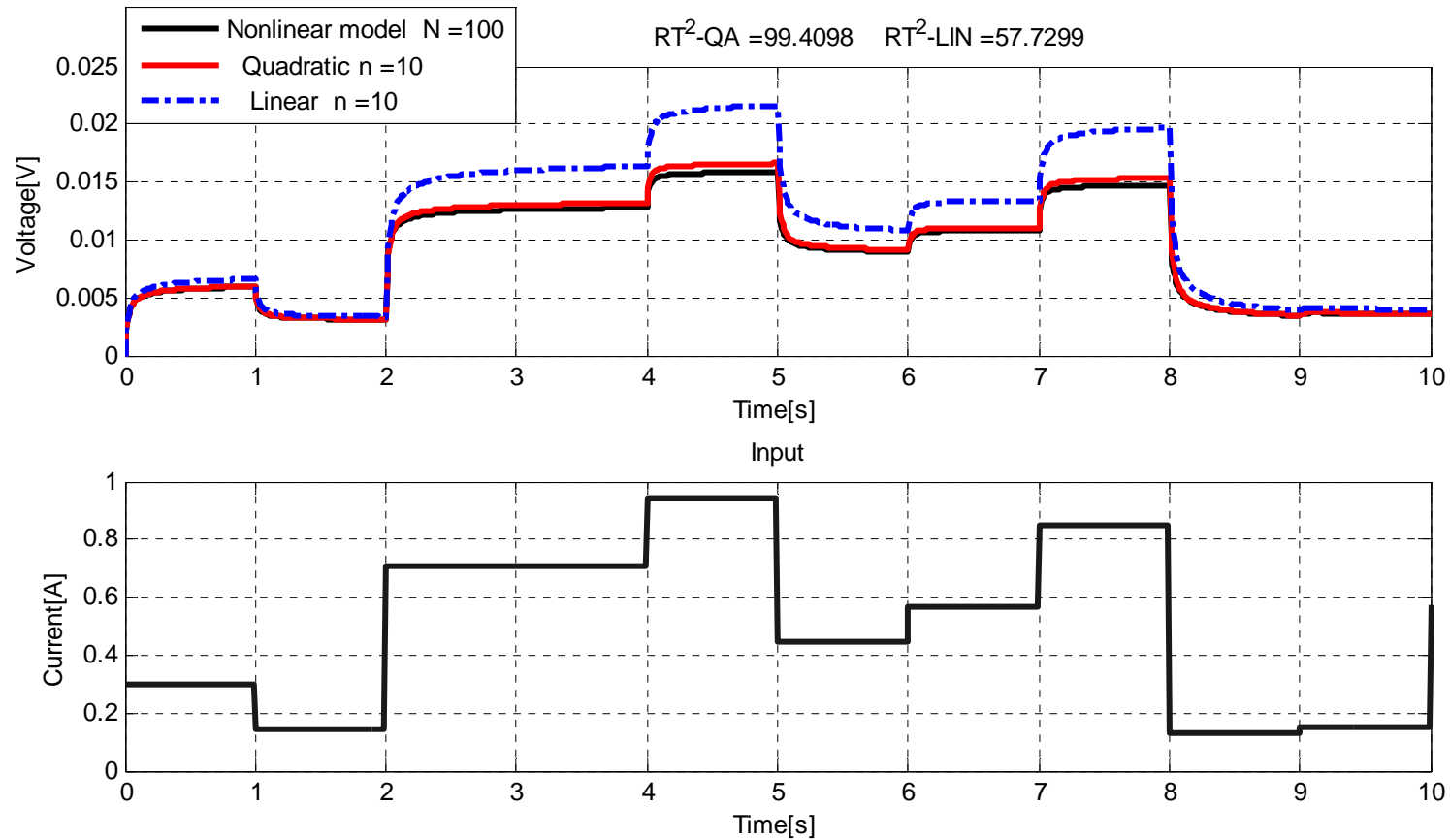
## Model parameters:

$$g(v) = e^{40v} + v - 1 \quad (\text{Nonlinear resistor profile})$$

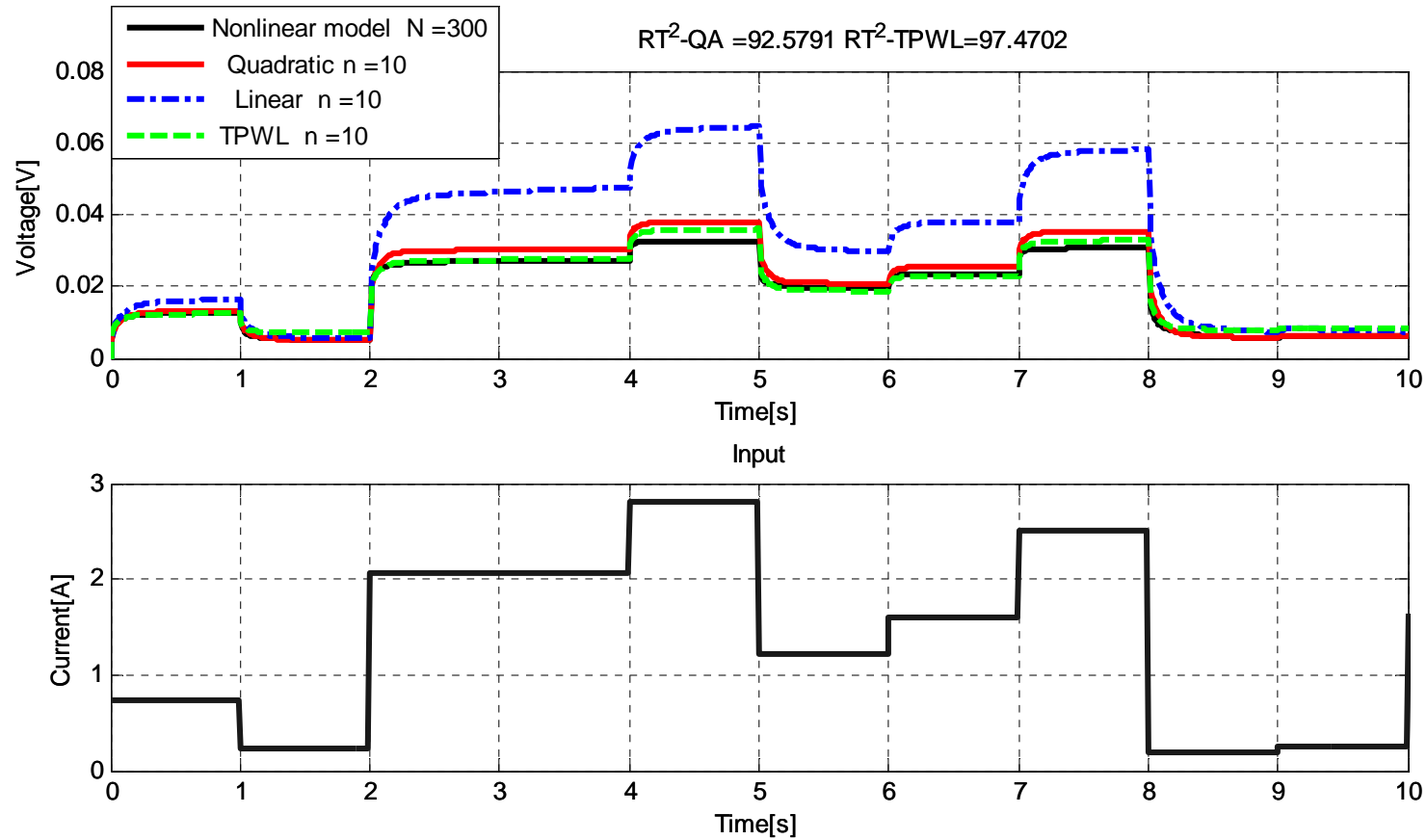
$$N = 100 \quad (\text{Number of branches})$$

$$C = 1$$

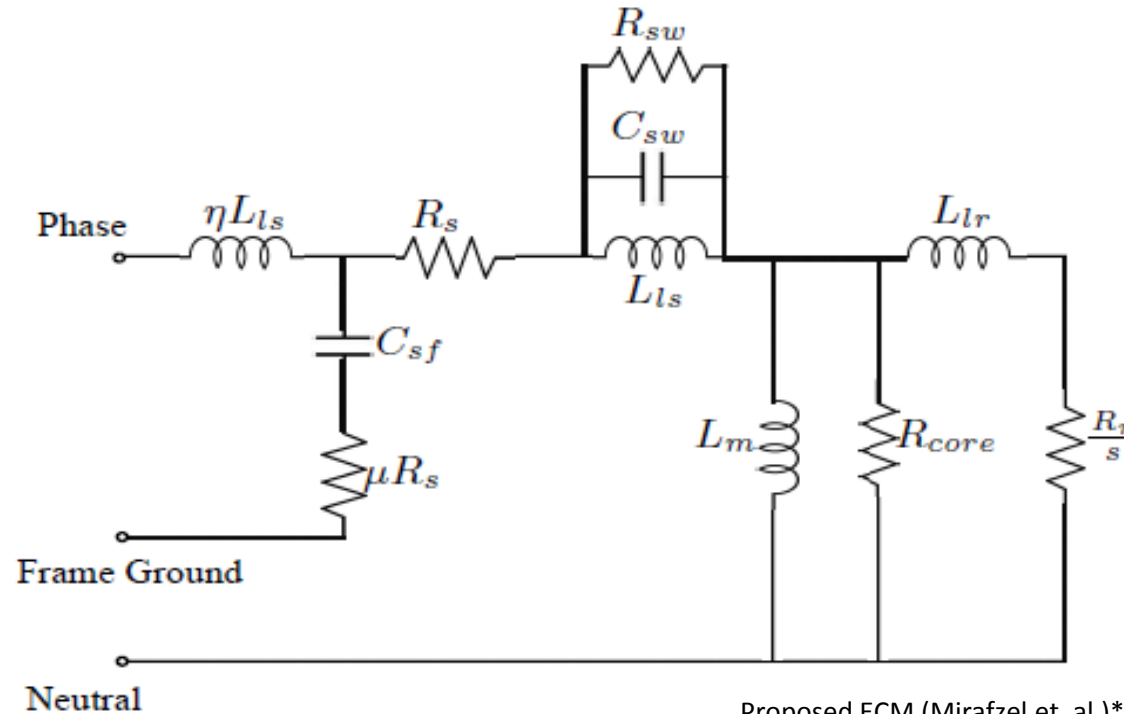
# Case study: Transmission line model



# Case study: Transmission line model



# Case study: Electric machine

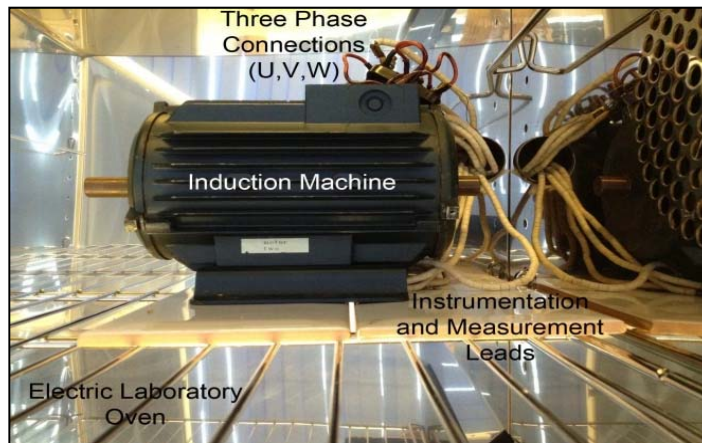


Proposed ECM (Mirafzel et. al.)\*

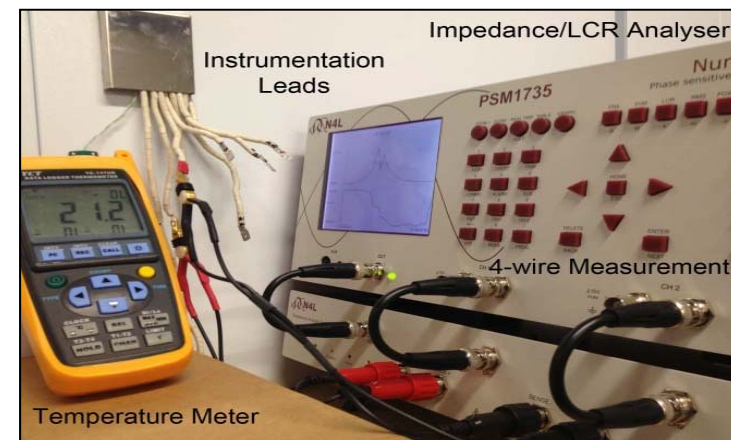
[\*] *B. Mirafzal, G.L. Skibinski, R.M. Tallam, D.W. Schlegel, and R.A. Lukaszewski. "Universal induction motor model with low-to-high frequency-response characteristics". IEEE Transactions on Industry Applications, 43(5), pp. 1233–1246, (2007).*

# Case study: Electric machine

- AC induction motor
- Thermal chamber
- Temperature data acquisition (DAQ)
- Temperature range: 22.4 °C – 210 °C with 20 °C increments
- NL4 precision impedance LCR analyser
- Frequency range of interest 100 Hz – 10 MHz



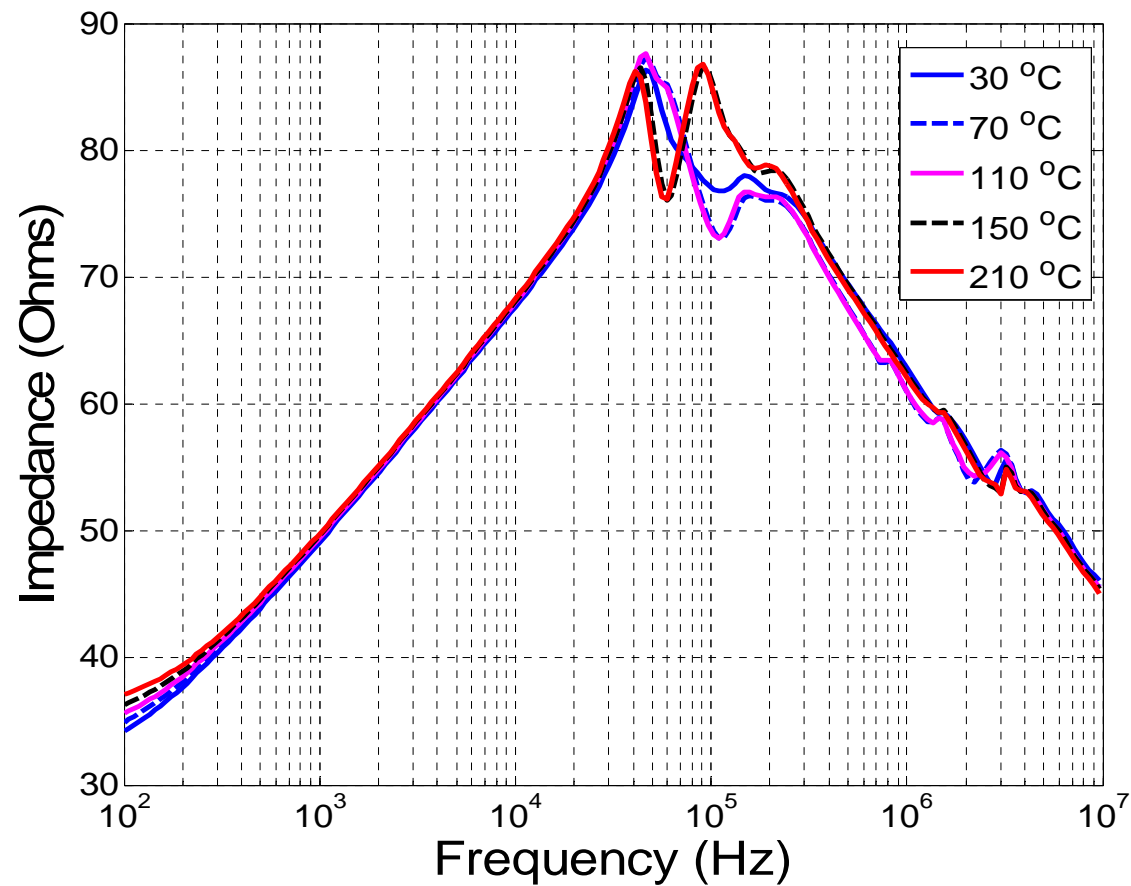
Induction machine inside electric oven



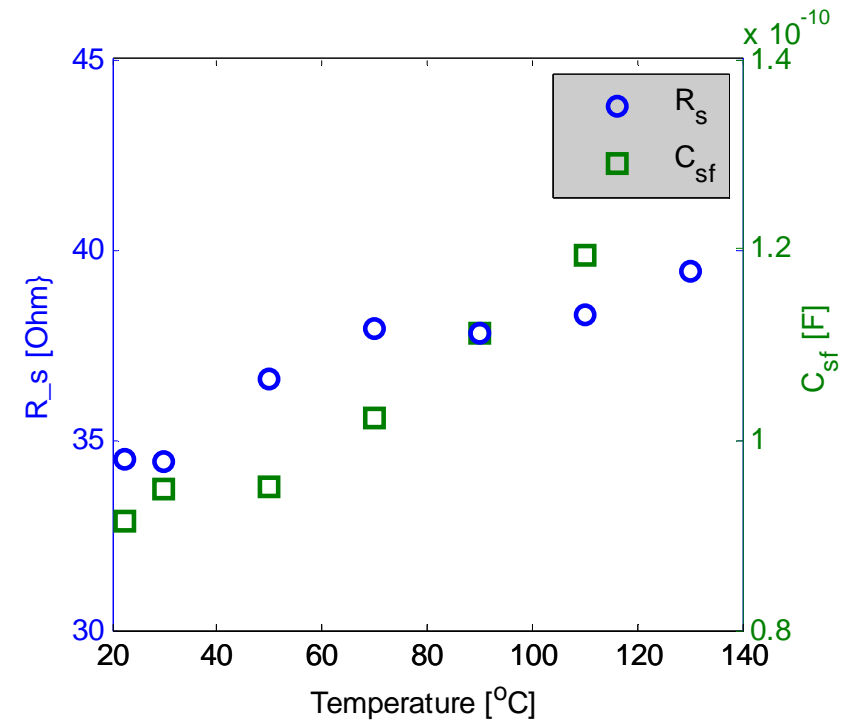
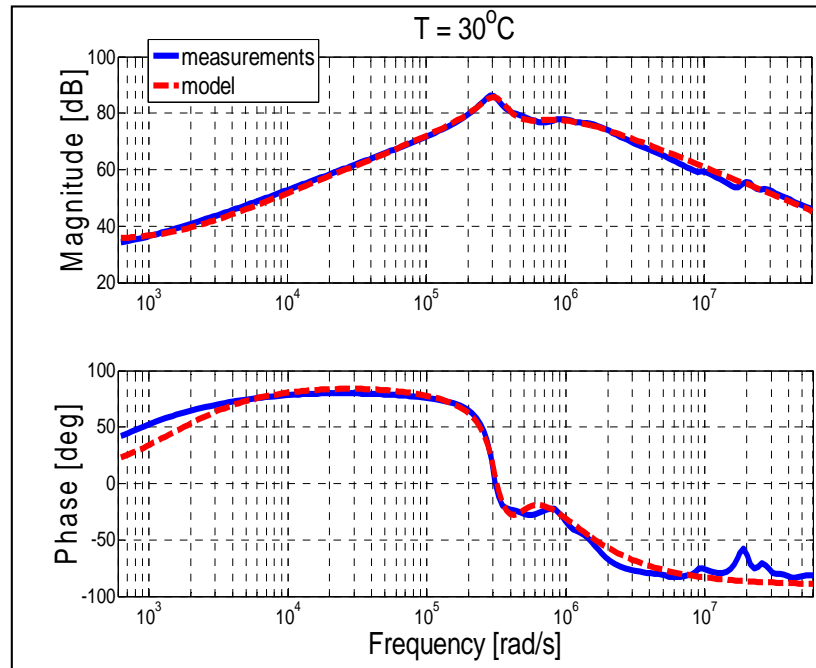
Impedance LCR analyser and temperature data logger

# Case study: Electric machine

Impedance measurements at different temperatures



# Case study: Electric machine



- ECM proven to be suitable for electric machine modelling up to 130  $^{\circ}$ C
- Nonlinear optimisation used to find temperature dependent parameters

# Case study: Battery



1. Data acquisition
  - > **Voltage** and **SOC** (outputs) responses to **current** input
  - > 36 short (80 seconds) data sets starting at different SOC (positive current input – charge mode)
  - > Experiment repeated for negative current (discharging)
2. Obtained set of 144 LTI models using simplified refined instrumental variable (SRIVC) method
  - > Current to SOC models
  - > Current to voltage models
3. **Assumption:** low order model can have linear structure, where parameters depend on SOC and sign of current



# Case study: Battery



- Observations:
  - > current to SOC transfer function does not depend on SOC neither on sign of current
    - transfer function described by linear 3<sup>rd</sup> order model

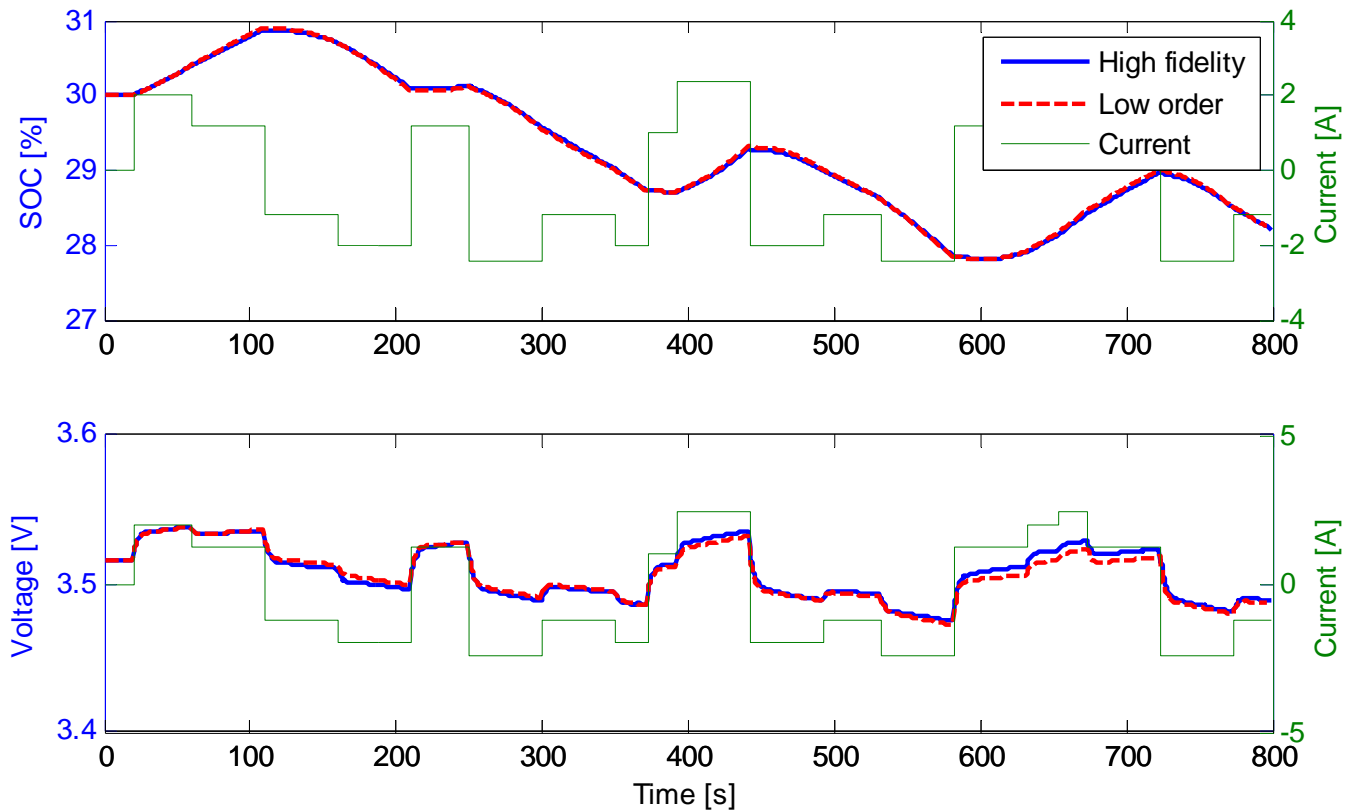
$$G_{soc}(s) = \frac{b_{11}s^2 + b_{21}s + b_{31}}{s^3 + a_{11}s^2 + a_{21}s + a_{31}}$$

- > current to voltage relationship depends on
  - SOC
  - sign of current

$$Z(s) = \frac{b_{02}(soc, m)s^2 + b_{12}(soc, m)s + b_{22}(soc, m)}{s^2 + a_{12}(soc, m)s + a_{22}(soc, m)} \quad m = \text{sign}(i(t))$$

- **Result:** 5<sup>th</sup> order piecewise state dependent parameter model
  - because model is piecewise – it can model hysteresis

# Case study: Battery



# Summary

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- Knowledge of the system/ high order model (features) as well as the purpose of reduced model (requirements) both define and inform the **reduction problem**
- A variety of techniques available for addressing model order reduction provides flexible approach to obtain models for specific purposes

Work to date:

- Techniques so far investigated are targeted towards control purposes

Further work:

- Models for diagnostics and prognostics also to be considered