

# Experimental and physics-based modeling assessment of strain induced mobility enhancement in FinFETs

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## Abstract

This study combines direct measurements of channel strain, electrical mobility measurements and a rigorous modeling approach to provide insight about the strain induced mobility enhancement in FinFETs and guidelines for the device optimization. Good agreement between simulated and measured mobility is obtained using strain components measured directly at device level by a novel technique. A large vertical compressive strain is observed in FinFETs and the simulations show that this helps recover the electron mobility disadvantage of the (110) FinFETs lateral interfaces w.r.t. (100) interfaces, with no degradation of the hole mobility. The model is then used to systematically explore the impact of the fin-width, fin-height and fin-length stress components on *n*- and *p*-FinFETs mobility and to identify optimal stress configurations.

## Introduction

FinFETs enable scaling of CMOS by enhancing electrostatic control [1, 2, 3], and strain is an important technology booster [3, 4, 5]. Strain induced mobility enhancement in planar MOSFETs has been studied extensively [6, 7, 8, 9], but the complex stress configurations in FinFETs, consisting of  $T_{fl}$ ,  $T_{fh}$  and  $T_{fw}$  components (see Fig.1), still demand physics-based models to support device design. In fact, so far the stress configurations in FinFETs have been typically inferred from process simulations and the analysis of mobility data has been based on the piezo-resistive coefficients [3, 4, 10], that offer limited insight and are inaccurate at high stress [11] and for complex stress configurations as in Fig.1. Furthermore, for narrow fins, mobility data is limited and strain measurement is challenging for established techniques [12, 13].

This paper presents an assessment of the strain induced mobility enhancement based on direct strain measurements, electrical mobility measurements and numerical physics-based modeling. Mobilities in narrow *n*- and *p*-FinFETs, measured from 77K to 300K, are compared with a state-of-the-art transport model based on the Boltzmann Transport Equation (BTE) in inversion layers, accounting for all the relevant scattering mechanisms, in which strain is implicitly introduced by modification of the band structure. Simulations are then used to

clarify the physical mechanisms for mobility enhancement and to provide guidelines for the device optimization.

## Device fabrication and characterization

22nm node FinFETs were fabricated using a VLSI-compatible process [1, 2] (Fig.2). Strain components  $\varepsilon_{zz}$ ,  $\varepsilon_{yy}$  ( $z$ ,  $y$  being the fin-height and fin-width directions, see DCS in Fig.1) of fully-processed devices were quantified directly by holographic interferometry [14, 15] (Figs.3 and 4). This novel technique is capable of measuring strain with nanometer spatial resolution and for relatively thick samples, thus suppressing the influence of sample relaxation. *Measured  $\varepsilon_{zz}$  is very large*, especially w.r.t. the low intrinsic stress of the TiN (Fig.5(a)), but it is consistent with strain induced by differences in thermal expansion coefficients following plastic relaxation at high temperature (Fig.5(b)).

Mobility was extracted in 10 $\mu$ m long, 65nm tall FinFET devices consisting of 10 fins in parallel by split  $C-V$  and  $I-V$  measurements. The drain current was measured at  $V_{DS}=10$ mV and corrected for gate leakage current, while the inversion charge  $N_{inv}$  was obtained by integration of the gate-to-channel capacitance curve; the channel area was obtained as  $10 \cdot L_{fin} \cdot (2H_{fin} + W_{fin})$ . Due to excessive gate leakage current, at  $N_{inv}$  larger than approximately  $2 \cdot 10^{13}$  cm<sup>-2</sup> the extracted mobility data were not considered to be reliable. Figs.6 and 7 compare the electron and hole mobility to literature data. *Electron mobility is significantly larger than for planar MOSFETs in the  $N_{inv}$  range of interest ( $\geq 2 \cdot 10^{12}$  cm<sup>-2</sup>)*. At low  $N_{inv}$  values the measured mobility shows a clear roll-off, stronger than in the reference data, most likely due to scattering by Coulomb centers in the high- $\kappa$  stack [16]. Hole mobility is comparable to literature data [17, 18, 20].

## Mobility model and validation

The transport analysis is focussed on the lateral (110)/(110) interfaces of the FinFETs simulated as double-gate devices. For a fin height of 65nm this assumption is appropriate for fin widths below approximately 20nm. The *n*-type devices were simulated with the Multi Subband Monte Carlo (MSMC) approach that accounts for the subband quantization and for the

most important scattering mechanisms [22]. Fig.8 shows a sketch of the  $\Delta_4$  and the  $\Delta_2$  valleys in a (110)/[110] electron inversion layer. In unstrained devices the  $\Delta_4$  valleys are the lowest due to the largest quantization mass  $m_y=0.315m_0$ . It has been argued that, due to the non parabolicity of the  $\Delta$  silicon valleys in the [110] direction, the parabolic effective mass approximation (EMA) is inaccurate for the  $\Delta_2$  valleys in (110) inversion layers [24]. We used a quantization model based on the Linear Combination of Bulk Bands (LCBB [25]) to extract a modified quantization mass  $m_{y,\text{eff}}=0.23m_0$  for the  $\Delta_2$  valleys, yielding good agreement of the EMA and the LCBB results [26]. Hole mobility was calculated starting from the band-structure obtained with a self-consistent  $\mathbf{k}\cdot\mathbf{p}$  solver coupled to the Poisson equation (as in [6, 7]), and then by using the momentum relaxation time approximation and accounting for phonons and surface roughness scattering by following [6]. All the scattering rates were calculated by using, for each subband, the envelope wave-function corresponding to  $\mathbf{k}=0$  [6]. The scattering parameters of Tab.1 were used for all the simulations of this paper. Figs.9 and 10 show good agreement between simulations and experiments for unstrained MOS-FETs.

The strain modeling starts by converting the  $T_{\text{FH}}$ ,  $T_{\text{FW}}$ ,  $T_{\text{FL}}$  stress components in the DCS to the corresponding strain tensor  $\varepsilon_c$  in the CCS (see Fig.1), by using appropriate rotation matrices and the silicon elastic compliance tensor. Then for electrons we calculated, for each strain tensor  $\varepsilon_c$ , the  $\Delta_4$  and the  $\Delta_2$  valley splitting and modulation of the effective masses using the results of [27], derived from a two band  $\mathbf{k}\cdot\mathbf{p}$  approach and validated against pseudo-potential calculations. These values were directly used in the MSMC simulations. For holes, instead, the  $\varepsilon_c$  enters directly the matrix of the  $\mathbf{k}\cdot\mathbf{p}$  calculations [6], hence the band-structure and the mobility determination; Fig.11 shows the strong deformation of the hole band-structure produced by the uniaxial stress. Figs.12, 13 show good agreement between simulations and experiments obtained for uniaxially strained (110)/ $\langle$ 110 $\rangle$  planar devices.

### Mobility in strained FinFETs

Mobility variations versus  $T_{\text{FL}}$ ,  $T_{\text{FH}}$  and  $T_{\text{FW}}$  are plotted in Figs.14, 15. Although qualitatively consistent, the piezo-resistive model yields large quantitative discrepancies w.r.t. the numerical simulations. Consistently with Figs.12, 13, tensile and compressive  $T_{\text{FL}}$  enhances electron and hole mobility, respectively. Furthermore a compressive  $T_{\text{FH}}$  increases the electron mobility, while it hardly affects hole mobility (see Tab.2).

To quantitatively investigate the effect of  $T_{\text{FH}}$ , Figs.16, 17 show that the mobility simulations obtained by using the measured strain values of Fig.4 are in fairly good agreement with measured data; in this respect, the DCS strain configuration of Figs.4 ( $\varepsilon_{zz}=-0.8\%$  and  $\varepsilon_{yy}=+0.3\%$ ) corresponds to a dominant  $T_{\text{FH}}$  stress component of approximately -1.1GPa. As for the interpretation of the electron mobility enhancements with compressive  $T_{\text{FH}}$ , Fig.8 shows that the  $\Delta_2$  valleys have a

smaller transport mass  $m_x$  than the  $\Delta_4$  valleys. Compressive  $T_{\text{FH}}$  yields a negative  $\Delta_2$  to  $\Delta_4$  valley splitting that improves the mobility through the re-population of the  $\Delta_2$  subbands (see Fig.18).

Figs.19 and 20 investigate the additivity of the  $T_{\text{FL}}$ ,  $T_{\text{FW}}$  and  $T_{\text{FH}}$  effects for mobility optimization. A tensile  $T_{\text{FL}}$  further improves electron mobility w.r.t. the values obtained with compressive  $T_{\text{FH}}$ , while a compressive  $T_{\text{FL}}$  increases the hole mobility. Fig.20 shows that the  $T_{\text{FW}}$  is not as effective as the  $T_{\text{FL}}$  for device optimization. Fig.19 and Fig.20 show that the piezo-resistive model results in quantitative and even qualitative discrepancies w.r.t. the numerical simulations and underlines the need for a rigorous modeling approach.

Finally, the additive effect of different strain components is experimentally confirmed by the stress induced  $I_{\text{DS}}$  improvements reported in Fig.21 for nano-scale FinFETs.

### Conclusions

In summary, direct strain measurements, mobility characterization and physics-based modeling were used to explain and optimize strain in both  $n$ - and  $p$ -type FinFETs. Our results assessed and explained the potentials for large electron mobility enhancements produced by the vertical strain and discussed the impact of all the main strain components on the electrical mobility. All the main simulation predictions were confirmed by experiments.

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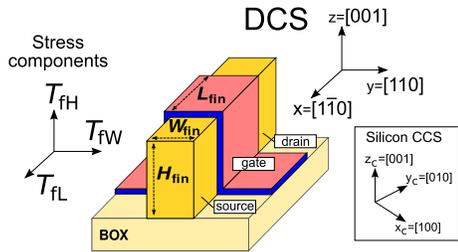


Figure 1: Schematic of a FinFET indicating the stress components in the fin height  $T_{fH}$ , width  $T_{fW}$  and length  $T_{fL}$  direction in the Device Coordinate System (DCS). Complex stress configurations comprising several  $T_{fH}$ ,  $T_{fW}$  and  $T_{fL}$  components may occur in the device. Also shown is the silicon Crystal Coordinate System (CCS).

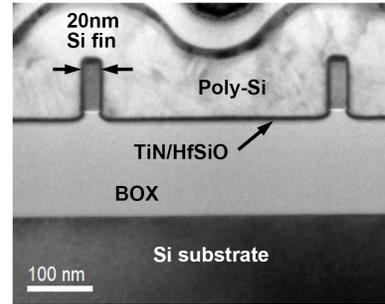


Figure 2: Cross-section TEM image through the gate-plane of FinFETs with  $W_{fin}=20nm$

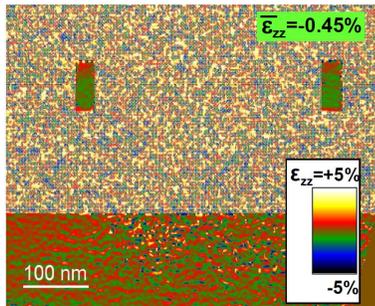


Figure 3: Direct measurement by holographic interferometry of deformation in vertical direction,  $\epsilon_{zz}$ , calculated from (004) fringes for 20nm wide fins (as pictured in Fig.2).

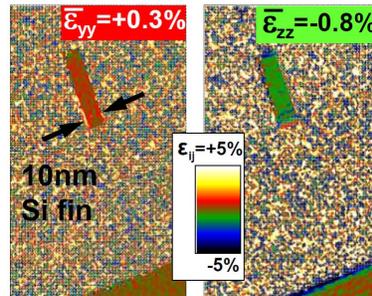


Figure 4: Deformation in (a) lateral ( $W_{fin}$ ) and (b) vertical ( $H_{fin}$ ) directions, calculated respectively from (111) and  $(\bar{1}\bar{1}\bar{1})$  holographic fringes for 10nm wide fins.

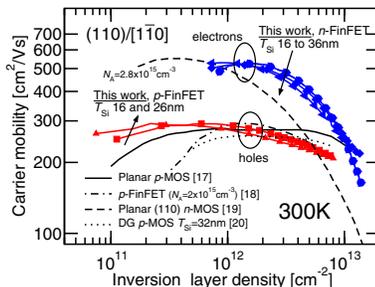


Figure 6: Measured electron and hole mobility at 300K for the  $n$ - and  $p$ -FinFETs of this work, compared to literature data for planar MOSFETs [17, 19, 20] or FinFETs [18]. All devices have very low channel doping concentrations below  $5 \times 10^{15} cm^{-3}$ .

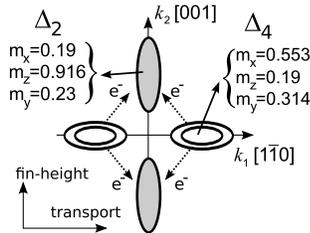


Figure 8:  $\Delta_4$  and  $\Delta_2$  valleys for the electrons in a (110)/[110] Si inversion layer. Mobility enhancements are obtained when stress forces the re-population of the  $\Delta_2$  valleys with the lowest mass  $m_x$  in the transport direction (see Fig.1).  $m_y$  is the quantization mass that enters the Schrödinger equation.

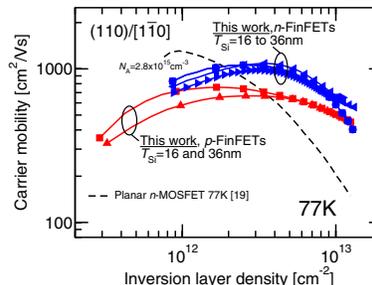


Figure 7: Measured electron and hole mobility at 77K for the  $n$ - and  $p$ -FinFETs of this work, compared to literature data for planar MOSFETs [19]. All devices have very low channel doping concentrations below  $5 \times 10^{15} cm^{-3}$ .

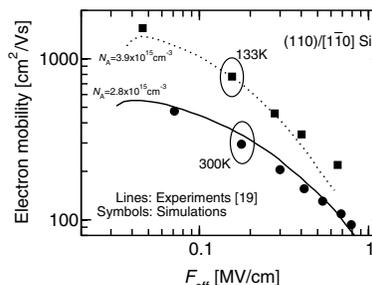


Figure 9: Simulated and experimental electron mobility (unstrained) versus effective field in (110) inversion layers, at 300K and 133K. Measurements from [19].

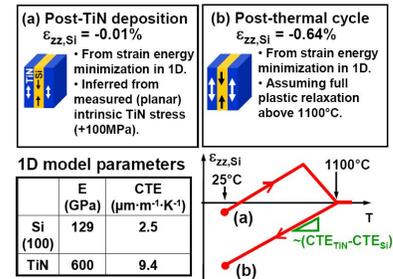


Figure 5: Maximum vertical strain  $\epsilon_{zz,Si}$  in Si fin (a) post-TiN deposition and (b) after thermal cycle. As-deposited strain is due to intrinsic stress in TiN and, for post-thermal cycle, to plastic relaxation at high temperature. CTE is the coefficient of thermal expansion and E is Young's modulus.  $W_{fin}=16nm$  and  $T_{TiN}=7nm$ .

Surface Roughness: (Exp. spectrum)	Holes	Electrons
$\Delta$ [nm]	0.24	0.9
$L_c$ [nm]	4	1.2
Phonons:	Holes	Electrons
Acoustic $D_{acc}$ [eV]	10.2	13
Optical $D_{opt}$ [ $10^8 eV/cm$ ]	15	from [23]
Optical Ph. Energy [meV]	62	from [23]

Table 1: Scattering parameters used in all simulations. Electron optical phonons model from [23]. Screening is not accounted for in the hole mobility calculations, hence the  $L_c$  is relatively large to reproduce the measured mobility vs.  $F_{eff}$  slope at large  $F_{eff}$  (see Fig.10).

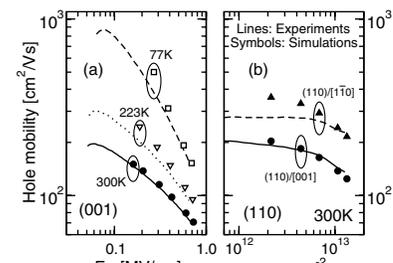


Figure 10: Simulated and experimental hole mobility (unstrained): (a) versus the effective field  $F_{eff}$  in (001) Si for different temperatures; (b) versus the inversion density in (110) Si. Measurements from [21] (a), [17] (b).

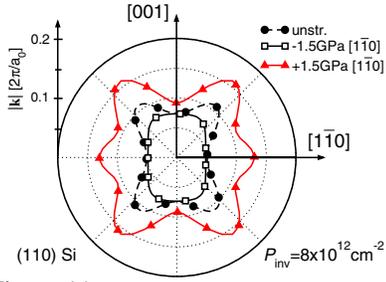


Figure 11: Hole equi-energy contour plots for the lowest subband at 100meV from the subband minimum for unstrained or strained (110) inversion layer.

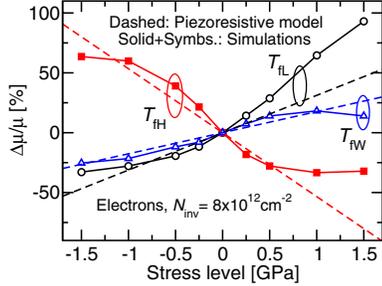


Figure 14: Simulated stress induced electron mobility variations vs.  $T_{FH}$ ,  $T_{FL}$ ,  $T_{FW}$  at  $N_{inv}=8 \times 10^{12} \text{ cm}^{-2}$  in (110) Si. Results are also shown for the piezo-resistive model with the bulk Si coefficients [28].

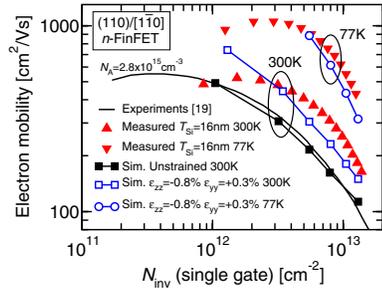


Figure 16: Measured and simulated electron mobility in  $n$ -FinFETs at 300K and 77K. Strain values  $\epsilon_{zz}=-0.8\%$  and  $\epsilon_{yy}=+0.3\%$  taken from Figs.4.

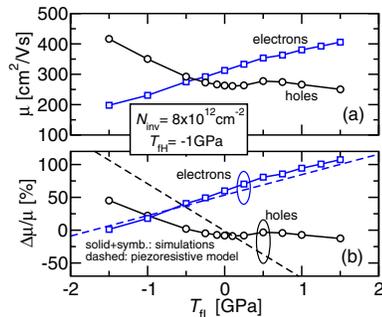


Figure 19: Simulated stress induced electron and hole mobility (a), and corresponding percentage mobility variations w.r.t. the unstrained case (b) vs.  $T_{FL}$  and for  $T_{FH}=-1\text{GPa}$ .

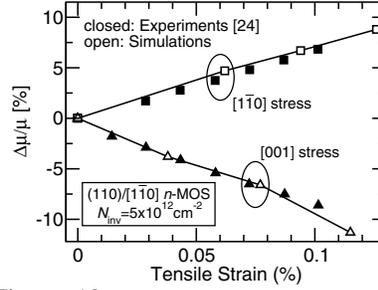


Figure 12: Simulations and measurements [24] of electron mobility variations in uniaxially strained (110)/(110) bulk planar  $n$ -MOSFETs.

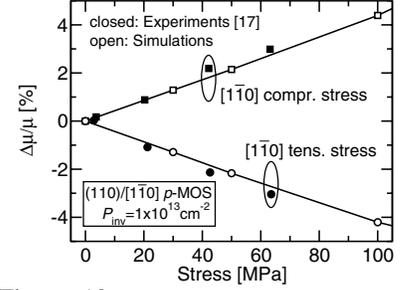


Figure 13: Simulations and measurements [17] of hole mobility variations in uniaxially strained (110)/(110) bulk planar  $p$ -MOSFETs.

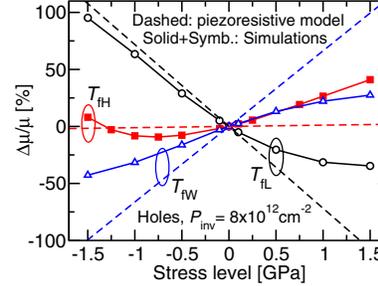


Figure 15: Simulated stress induced hole mobility variations vs.  $T_{FH}$ ,  $T_{FL}$ ,  $T_{FW}$  at  $P_{inv}=8 \times 10^{12} \text{ cm}^{-2}$  in (110) Si. Results are also shown for piezo-resistive model with the bulk Si coefficients [28].

		Compressive			Tensile		
		$T_{fL}$	$T_{fW}$	$T_{fH}$	$T_{fH}$	$T_{fW}$	$T_{fL}$
Electron mobility		↘	↘	↗	↘	↗	↗
Hole mobility		↗	↘	=	↗	↗	↘

FinFET stress components:  $T_{FH}$ : fin-height,  $T_{fW}$ : fin-width,  $T_{fL}$ : source-drain

Table 2: Table summarizing the impact of different stress components on the electron and hole (110)/[110] FinFETs mobility.

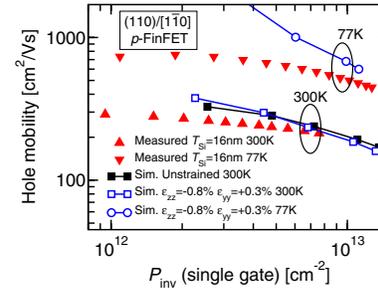


Figure 17: Measured and simulated hole mobility in  $p$ -FinFETs at 300K and 77K. Strain values  $\epsilon_{zz}=-0.8\%$  and  $\epsilon_{yy}=+0.3\%$  taken from Figs.4.

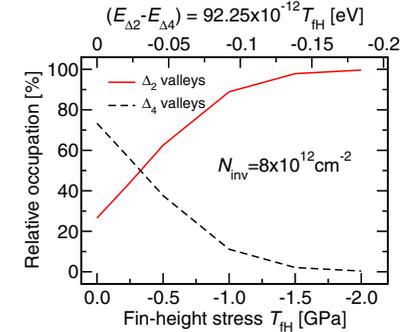


Figure 18: Simulated re-population of the  $\Delta_2$  valleys in (110)/[110]  $n$ -FinFET vs. compressive  $T_{FH}$  (bottom  $x$ -axis). The top  $x$ -axis shows the stress induced  $\Delta_2$  to  $\Delta_4$  valley splitting that concurs with the quantization to the overall subbands splitting.

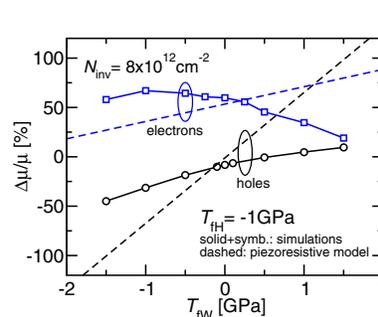


Figure 20: Simulated stress induced electron and hole percentage mobility variations w.r.t. the unstrained case vs.  $T_{FW}$  and for  $T_{FH}=-1\text{GPa}$ .

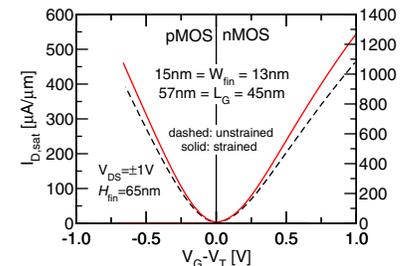


Figure 21: Influence of additional uniaxial  $\epsilon_{xx}$  strain upon  $I_{D,Sat}$  in FinFETs. Strain induced by  $\text{epi-Si}_{1-x}\text{Ge}_x$  S/D for  $p$ -MOS and by wafer bending for  $n$ -MOS.  $I_{D,Sat}$  is boosted by 13% for  $p$ -MOS with  $\chi=25\%$  and by 21% for  $n$ -MOS with 460MPa stress. Uniaxial strain boosters are thus effective in presence of large  $\epsilon_{zz}$ .